

**LEARNING MATERIAL OF
STRUCTURAL DESIGN - I**

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27 April 2021

1st chapter

R.C.C (Reinforced cement concrete) :-

- It is the mixture of cement coarse aggregate, fine aggregate steel bar & water within proportional limits.
- Reinforced concrete also called Reinforced Cement concrete.
- A composite materials in which concrete relatively low tensile strength & ductility are compensated by the inclusion of reinforcement having higher tensile strength & ductility.

Objectives of design & detailing

Every structure must be designed to satisfy a basic requirement.

(1) Stability :- To prevent overturning, sliding or buckling of the structure or parts of it, under the action of loads.

(2) Strength :- To resist safely the stresses induced by the loads in the various structural members.

(3) Serviceability :- To ensure satisfactory performance under service load conditions which implies providing adequate deflection, crack width

& vibrations within in acceptable limits & also providing impermeability, durability etc.

Advantages of R.C.C

The following are the major advantages of R.C.C.

- Reinforced concrete has good compressive stress because of concrete.
- RCC also has high tensile stress because of steel.
- It has good resistance to damage by fire & weathering.
- R.C.C protects steel bars from buckling & twisting at the high temperature.
- R.C.C prevent steel from rusting.
- R.C.C is durable.

Disadvantages of R.C.C :-

- (1) The tensile strength of reinforced concrete is about tenth of its compressive strength.
- (2) The main steps of using reinforced concrete are mixing, casting & curing. All of these affect the final strength.
- (3) The cost of forms used for casting is relatively higher.
- (4) shrinkage causes crack development & strength loss.

Different methods of design :-

- (1) Working stress method (W.S.M)
- (2) Ultimate load method (U.L.M)
- (3) Limit state method (L.S.M)

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(1) Working stress method :- (W.S.M)

→ In India, before 1964, most of the structures were designed by working stress method.

→ In working stress method it is assumed that concrete & steel are elastic. At the worst combination of working loads the stresses in materials are not exceeded beyond permissible stresses.

(2) Ultimate load method (U.L.M)

→ The second revision of IS 456 introduced ultimate load method of design. It gave more economical section than W.S.M

(3) Limit state method (L.S.M)

The third revision of IS 456 introduced limit state method of design.

→ Limit state method has become very popular & most of the structures are now designed by limit state method.

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Working stress method

Permissible stress:- In working stress method the stresses in materials are not exceeded beyond their permissible value.

permissible stress in concrete:-

Grade of concrete

permissible stress in
compression N/mm^2
(σ_{cbc})

M20 \longrightarrow 7 N/mm^2

M25 \longrightarrow 8.5 N/mm^2

M30 \longrightarrow 10 N/mm^2

[minimum grade of concrete \rightarrow M20]

Grade / Types of steel

(i) mild steel \longrightarrow Fe 250

(ii) HYSD steel (High yield strength Deformed bar)

\longrightarrow Fe 415

Grade of steel

(σ_{st}) N/mm^2

Fe 250 \longrightarrow ~~250~~ 140 N/mm^2

Fe 415 \longrightarrow ~~415~~ 230 N/mm^2

Fe 500 \longrightarrow 300 N/mm^2

Fe 250 \longrightarrow $\frac{F_{ck}}{2.5}$ 250 N/mm^2

Fe 415 \longrightarrow $\frac{F_{ck}}{1.25}$ 415 N/mm^2

Modular Ratio (m) :-

It is defined as the ratio of modulus of elasticity of steel to modulus of elasticity of concrete.

$$\therefore m = \frac{E_s}{E_c} \quad E_s = 2 \times 10^5 \text{ N/mm}^2$$

$$m = \frac{280}{3\sigma_{cbc}}$$

σ_{cbc} = permissible stress in concrete.

Q Find modular ratio of M20 grade concrete?

Solⁿ Grade of concrete = M20

$$m = \frac{280}{3\sigma_{cbc}}$$

$$\sigma_{cbc} = 7 \text{ N/mm}^2$$

$$m = \frac{280}{3 \times 7} = 13.33$$

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u.v.v.p

Assumption :-

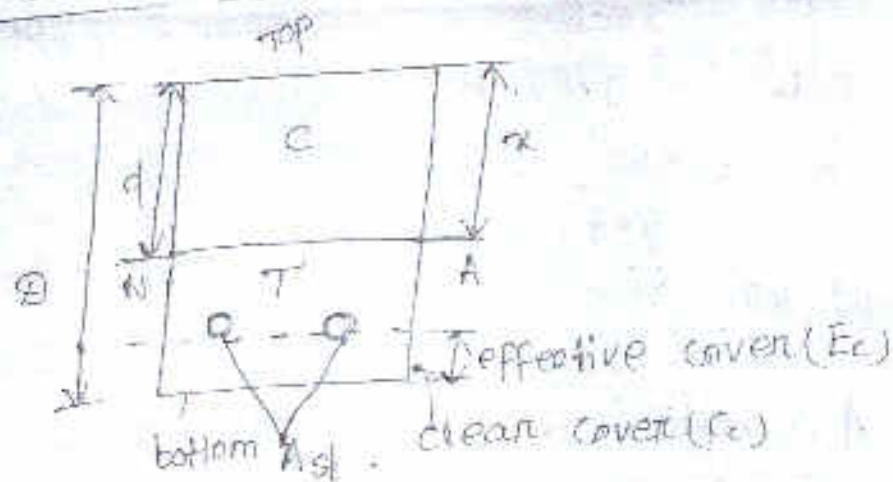
- (1) At any cross-section, plane section before bending remain plane after bending.
- (2) All tensile stresses are taken up by reinforcement & none by concrete.
- (3) The stress-strain relationship of steel and concrete under working loads is a straight line.

- (4) There exist a perfect bond between steel & concrete.
- (5) The modular ratio m has the value $\frac{280}{3\sigma_{bc}}$, where σ_{bc} = permissible stress in concrete.
- (6) Concrete is assumed to be homogeneous.

Types of beam

- (i) Singly reinforced beam
- (ii) Doubly reinforced beam

singly reinforced beam -



D = overall depth

It is the distance between top fibre to bottom fibre of beam

effective depth (d)

It is the distance between top fibre of beam to 'centroid' of steel bar.

Effective cover (E_c)

It is distance between centroid of bars to bottom of the beam.

Clear cover (C_c)

It is distance between bottom of bar to bottom of beam.

Types of Section

(i) Balance section

(ii) under reinforced section

(iii) over reinforced section

(1) Balance reinforced section :-

When the maximum stresses in steel and concrete simultaneously reach their allowable value, the section is said to be balanced section.

$$x = x_{bal}$$

Area of steel = Area of balance

(2) Under reinforced section :-

→ When % of steel in a section is less than required for a balanced section, the section is called under reinforced section.

→ In this case concrete stress doesn't reach its maximum allowable value while the stress in steel reached its maximum permissible

$$\alpha_{bal} > \alpha, A_{st, bal} > A_{st}$$

Over reinforced section :-

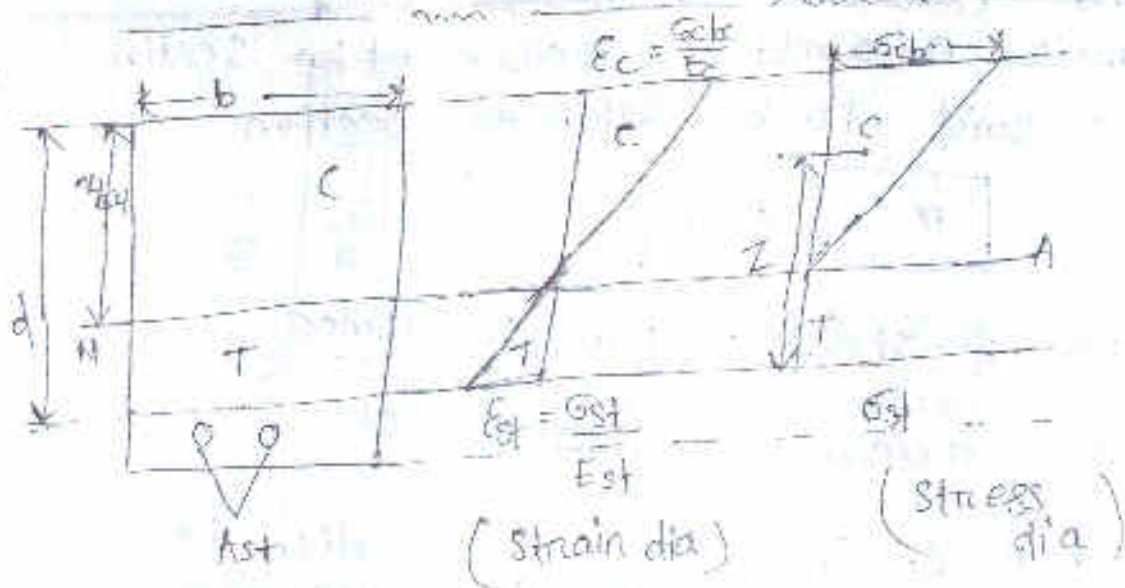
when the % of steel in a section is more than that required for a balance section, the section is called over reinforced section.

⇒ In this case the stress in concrete reaches its maximum allowable value earlier than that in steel.

$$\alpha_{bal} < \alpha, A_{st, bal} < A_{st}$$

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Derivation of formula for balance section :-



$A_{st, bal}$ = Area of steel in balance section

$\sigma_{c, bc}$ = permissible stress in concrete in compression.

σ_{st} = permissible stress in steel in tension.

E_c = Modulus of elasticity of concrete.

E_{st} = Modulus of elasticity of steel.

Z = Lever Arm

It is defined as the distance between centroid of compression force to centroid of tensile force.

b = width of the beam.

x = N.A depth

To find neutral Axis

$$\text{From the strain dia } \frac{x_{bal}}{d - x_{bal}} = \frac{\sigma_{cbc} / \epsilon_c}{\sigma_{st} / \epsilon_{st}}$$

$$\Rightarrow \frac{x_{bal}}{d - x_{bal}} = \frac{\sigma_{cbc}}{\epsilon_c} \times \frac{\epsilon_{st}}{\sigma_{st}}$$

$$\Rightarrow \frac{x_{bal}}{d - x_{bal}} = \frac{\sigma_{cbc}}{\sigma_{st}} \times \frac{\epsilon_{st}}{\epsilon_c}$$

$$\Rightarrow \frac{x_{bal}}{d - x_{bal}} = \frac{\sigma_{cbc} \times m}{\sigma_{st}}$$

$$\Rightarrow \frac{x_{bal}}{d - x_{bal}} = \frac{m \sigma_{cbc}}{\sigma_{st}}$$

$$\Rightarrow x_{bal} (\sigma_{st}) = (d - x_{bal}) (m \sigma_{cbc})$$

$$\Rightarrow x_{bal} (\sigma_{st}) = d m \sigma_{cbc} - m x_{bal} \sigma_{cbc}$$

$$\Rightarrow x_{bal} \sigma_{st} + x_{bal} m \sigma_{cbc} = m \sigma_{cbc} d$$

$$\Rightarrow x_{bal} (\sigma_{st} + m \sigma_{cbc}) = m \sigma_{cbc} d$$

$$\Rightarrow x_{bal} = \frac{m \sigma_{cbc} d}{\sigma_{st} + m \sigma_{cbc}}$$

$$\Rightarrow \alpha_{bal} = \left(\frac{m_{scbc}}{m_{scbc}} \right) d \left(\frac{\sigma_{st}}{m_{scbc}} + \frac{m_{scbc}}{m_{scbc}} \right)$$

$$\Rightarrow \alpha_{bal} = d \left(\frac{1}{1 + \frac{\sigma_{st}}{m_{scbc}}} \right)$$

$$\boxed{\alpha_{bal} = kd}$$

where $k = \frac{1}{1 + \frac{\sigma_{st}}{m_{scbc}}}$

To find out Lever Arm z

$$z = d - \frac{\alpha_{bal}}{3}$$

$$= d - \frac{kd}{3}$$

$$= d \left(1 - \frac{k}{3} \right)$$

$$= dj$$

$$\boxed{z = dj}$$

where $j = 1 - \frac{k}{3}$

$$\boxed{\begin{array}{l} j - \text{Lever Arm constant} \\ k - \text{Neutral Axis} \end{array}}$$

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To find total forces :-

$C = \text{Total compression}$

$T = \text{Total tension}$

$$C = T$$

$$C = \sigma_{cbc} \times \frac{1}{2} \times b \times x_{bal}$$

$$C = \frac{\sigma_{cbc} \times b \times x_{bal}}{2}$$

force in compression zone

$$T = \sigma_{st} \times A_{stbal}$$

$$T = \sigma_{st} \times A_{stbal}$$

force in tension zone.

To find out moment of resistance of the section (MR)

Capacity of a section to resist the moment is known as its moment of resistance.

$M_R = \text{Total com. force} \times LA$ or total tensile force $\times LA$ (whichever is small)

For balanced section $C = T$ so both will have same volume

$$M_R = \left(\frac{1}{2} \sigma_{cbc} \times x_{bal} \times b \right) \times j d$$

$$= \left(\frac{1}{2} \times \sigma_{cbc} \times x_{bal} \times b \right) j d$$

$$= \left(\frac{1}{2} \sigma_{cbc} \times x_{bal} \right) b j d$$

$$M_R = Q_{bal} \times b d^2$$

where $Q_{bal} = \frac{1}{2} \sigma_{cbc} k j$

Considering tensile forces

$$F_T = \text{total tension} \times l \cdot A$$

$$MR \text{ or } M_{bal} = f_{st} A_{st} b d_j$$

To find steel area :-

$$M_{bal} = f_{st} A_{st} j d$$

$$\Rightarrow A_{st} = \frac{M_{bal}}{f_{st} j d}$$

P_t bal (percentage of balance)

$$P_t \text{ bal} = \frac{50k f_{st} b c}{f_{st}}$$

To design balanced section :-

For a given design moment 'M', $M = M_{bal}$; if w_k of the given or assumed

$$d = \frac{M_{bal}}{Q_{bal} x b}$$

$$\text{Steel area } A_{st} = A_{st} \text{ bal} = \frac{M}{f_{st} j d}$$

Q6

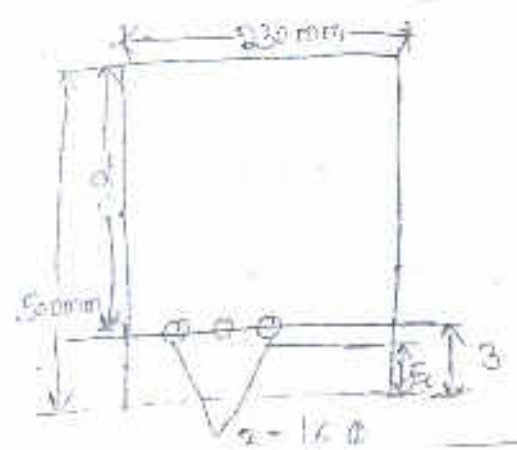
Determine the effective depth of the beam section :-

$$Q = 500 \text{ mm}$$

$$d_{st} = 16 \text{ mm}$$

$$d = 9$$

$$d = Q - c_c - \frac{d_{st}}{2}$$



$$= 500 - 30 - \frac{16}{5}$$

$$= 500 - 30 - 8 = 462 \text{ mm.}$$

26 Calculate the design constants for the following balanced design for singly reinforced section. The materials are grade M20 concrete & mild steel reinforcement. Considering the

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Given data :-

For M20 grade concrete $\sigma_{cbc} = 7 \text{ m.}$

Mild steel $\sigma_{st} = 140 \text{ N/mm}^2$

$$m = \frac{280}{3\sigma_{cbc}} = \frac{280}{3 \times 7} = 13.33$$

Neutral Axis constant (K)

$$K = \frac{1}{1 + \frac{\sigma_{st}}{m\sigma_{cbc}}}$$

$$= \frac{1}{1 + \frac{140}{13.33 \times 7}} = 0.430$$

Lever arm constant (j)

$$j = 1 - \frac{K}{3}$$

$$= 1 - \frac{0.4}{3} = 0.87$$

MR constant (R_{bal})

$$R_{bal} = \frac{1}{2} \times \sigma_{cbc} \times k \times j$$

$$= \frac{1}{2} \times 7 \times 0.4 \times 0.87$$

$$= 1.91$$

$$(P_t)_{bal} = \frac{50 \sigma_{bc} k}{\sigma_{st}}$$

$$= \frac{50 \times 7 \times 0.4}{1.91} = 1$$

Q For a rectangular beam of size 250mm wide \times 520mm effective depth, find out the balance depth of NA, balance lever arm, balanced MR, balanced steel area, the materials are M20 grade concrete & HYSD reinforcement of grade Fe 415.

Given data :-

width of the beam (b) = 250 mm

Effective depth (d) = 520 mm

For M20 grade concrete $\sigma_{cbc} = 7 \text{ N/mm}^2$

For Fe 415 grade steel $\sigma_{st} = 230 \text{ N/mm}^2$

Solⁿ 1) To find out Neutral Axis depth (x_{bal})

$$x_{bal} = k \cdot d$$

$$k = \frac{1}{1 + \frac{\sigma_{st}}{m \sigma_{cbc}}}$$

$$= \frac{1}{1 + \frac{230}{13.33 \times 7}}$$

$$= 0.29$$

$$x_{bal} = kd$$

$$= 0.29 \times 520 = 150.8 \text{ mm}$$

$$M = \frac{280}{3 \times 7} = 13.33$$

ii) Level of Arm (z)

$$z = dj$$

$$j = 1 - \frac{k}{3}$$

$$= 1 - \frac{0.29}{3} = 0.9$$

$$z = 520 \times 0.9 = 468 \text{ mm}$$

iii) Moment of Resistance (MR)

$$MR = Q_{bal} \times b d^2$$

$$Q_{bal} = \frac{1}{2} \times \sigma_{cbc} \times k \times j$$

$$= \frac{1}{2} \times 7 \times 0.29 \times 0.9$$

$$= 0.91$$

$$MR = 0.91 \times 250 \times 520^2$$

$$= 61516 \text{ N}\cdot\text{mm}$$

$$= 61.51 \text{ kN}\cdot\text{m}$$

$$A_{st, bal} = \frac{P_{t, bal} \times b d}{100}$$

$$P_{t, bal} = \frac{50 \text{ c/c} \times k}{150} = \frac{50 \times 7 \times 0.29}{230}$$

$$= 0.44$$

$$A_{st, bal} = 0.44 \times 250 \times 520$$

$$= \frac{57200}{100} = 572 \text{ mm}^2$$

Cone. grade	Steel grade	σ_{bc}	σ_{st}	k	j	Q_{bal}	P_{bal}
M20	Fe 250	7	140	0.4	0.87	1.21	1
M20	Fe 415	7	230	0.29	0.89	0.91	0.144

Q. A simply supported rectangular beam of 4m span carries a uniform distributed load of 26 kN/m. The width of the beam is 230 mm. Find the depth & steel area for the balanced design. Use M20 grade concrete & mild steel reinforcement.

Given data

$$\text{Span length } (L) = 4 \text{ m}$$

$$w = 26 \text{ kN/m}$$

$$\text{moment} = \frac{wL^2}{8}$$

$$= \frac{26 \times 4^2}{8} = 52 \text{ kNm}$$

$$d = \sqrt{\frac{M}{Q_{bal} b}}$$

$$= \sqrt{\frac{52 \times 10^6}{1.21 \times 230}} = 432.26 \approx 432.3 \text{ mm}$$

$$\text{Steel area } A_{st, bal} = \frac{M}{\sigma_{st} j d}$$

$$= \frac{52 \times 10^6}{140 \times 0.87 \times 432.3}$$

$$= 987.57 \text{ mm}^2$$

$$\approx 988 \text{ mm}^2$$

$$A_{st} = 988 \text{ mm}^2$$

Assume 5 no of bars 16mm dia

$$\text{Area} = 5 \times \frac{\pi}{4} \times 16^2$$

$$= 1005 \text{ mm}^2$$

Provide 5 no of 16mm dia bar

$$\text{Assume } C_c = 30 \text{ mm}$$

Effective cover

$$= \frac{16}{2} + C_c$$

$$= 8 + 30 = 38 \text{ mm}$$

Overall depth

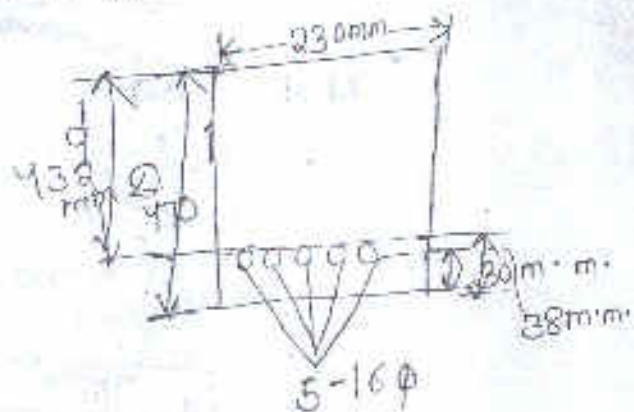
$$D = \text{dt Effective cover}$$

$$= 432 + 38 = 470.3 \text{ mm}$$

$$D = 470 \text{ mm}$$

$$d = 470 - 38 = 432 \text{ mm}$$

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1.8

For a rectangular beam of size 250mm wide x 520mm effective depth. Find out the balance depth of n-t, balance lever arm, balanced, n-t balanced steel area, the materials are M25 grade concrete & HYSD reinforcement of grade Fe 250.

Given data:-

Width of beam (b) = 250 mm

Effective depth (d) = 520 mm

M25 grade concrete $\sigma_{bc} = 8.5 \text{ N/mm}^2$

Fe 250 grade steel $\sigma_{st} = 140 \text{ N/mm}^2$

(i) Neutral Axis balance

$$x_{bal} = kd$$

$$M = \frac{280}{3 \times 8.5} = 10.98$$

$$k = \frac{1}{1 + \frac{\sigma_{st}}{m \sigma_{bc}}}$$

$$= \frac{1}{1 + \frac{140}{10.98 \times 8.5}}$$

$$= 0.39$$

$$x_{bal} = 0.39 \times 520 = 202.8 \text{ mm}$$

(ii) Lever Arm (z) = dj

$$j = 1 - \frac{k}{3} = 1 - \frac{0.39}{3} = 0.87$$

$$z = 0.87 \times 520 = 452.4 \text{ mm}$$

$$= 0.8 \times 520 = 416 \text{ mm}$$

(iii) MR constant (R_{bal})

$$MR = R_{bal} \times b d^2$$

$$= \frac{1}{2} \times 8.5 \times 0.39 \times 0.87$$

$$= 1.44$$

$$MR = 1.44 \times 250 \times 520^2$$

$$= 9734 \text{ Nmm} = 97.34 \text{ Nmm}$$

$$A_{st\ bal} = \frac{P_{t\ bal} \times b \times d}{100}$$

$$P_{t\ bal} = \frac{505 \text{ bck}}{69}$$

$$= \frac{50 \times 8.5 \times 0.639}{140} = 1.183$$

$$A_{st\ bal} = \frac{1.18 \times 250 \times 520}{100}$$

$$= 1534 \text{ mm}^2$$

Q2 A simply supported rectangular beam of 6m span carries a u.d.l of 36 kN/m. The width of the beam is 230 mm. Find the depth & steel area for the balanced design. Use M20 grade concrete & mild steel reinforcement.

Ans Given data:-

span length = 6m

u.d.l = 36 kN/m

width of beam = 230 mm

$$\text{Moment} = \frac{w \cdot l^2}{8}$$

$$= \frac{36 \times 6^2}{8} = 162 \text{ kNm}$$

$$d = \sqrt{\frac{M}{0.85 \times 12.1}} = \sqrt{\frac{162 \times 10^6}{1.02 \times 230}} = 762.95 \text{ mm}$$

$$= 762.9 \text{ mm}$$

$$\text{steel area } A_{st} \text{ bal} = \frac{M}{\sigma_{st} j d}$$

$$= \frac{1.62 \times 10^6}{140 \times 0.87 \times 762.9}$$

$$= 1743.41$$

$$A_{st} \text{ bal} = 1743 \text{ mm}^2$$

Assume 6 no of bar 20 m.m diameter.

$$\text{Area} = 6 \times \frac{\pi}{4} \times 20^2$$

$$= 1884.9 \text{ mm}^2$$

Assume $C_c = 30 \text{ m.m.}$

$$\text{Effective cover} = \frac{20}{2} + C_c$$

$$= \frac{20}{2} + 30 = 40 \text{ m.m.}$$

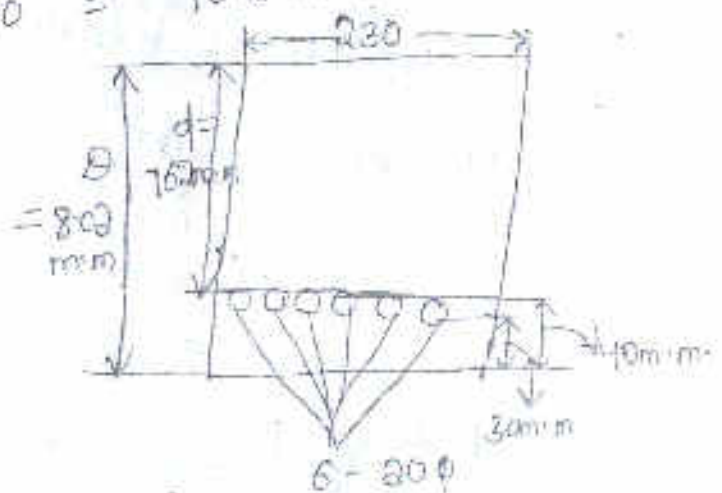
overall depth (D)

$$= d + \text{Effective cover}$$

$$= 762.9 + 40$$

$$= 802.9 \text{ m.m.}$$

$$d = 802 - 40 = 762 \text{ m.m.}$$



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$$\begin{aligned} \% \text{ of steel } (P_t) &= \frac{100 A_{st}}{b d} \\ &= \frac{100 \times 1005}{230 \times 232} \\ &= 1.883 \end{aligned}$$

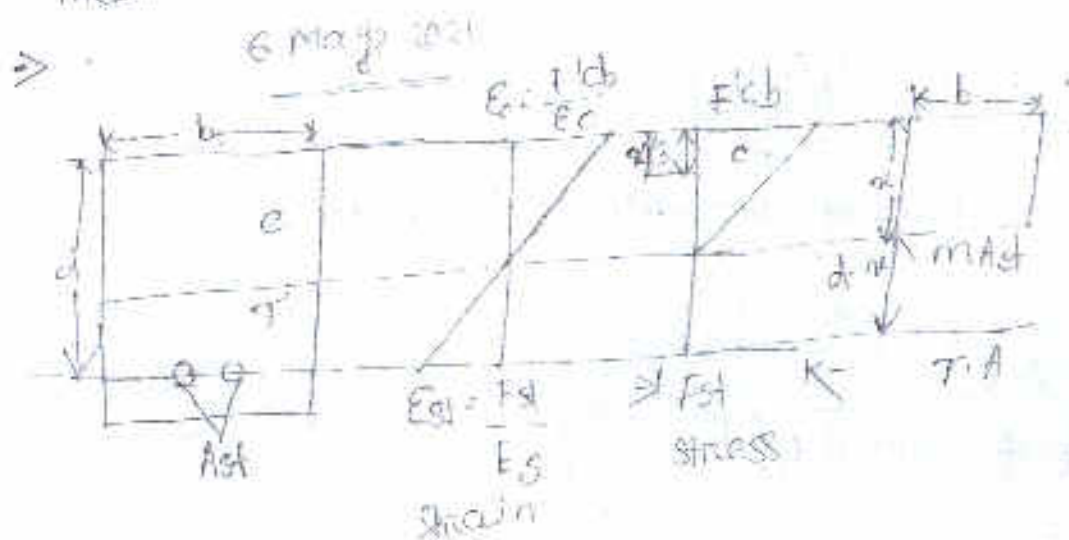
$$(P_t)_{bal} = 1$$

$$P_t < (P_t)_{bal}$$

So, it is O.R.'S

Transformed Area method

- A transformed section is a section in which the steel area is replaced by an equivalent concrete area.
- A transformed section consist of a single material, therefore theory of simple bending is applied.
- The transformed area may be steel when concrete is replaced or concrete when steel is replaced by concrete.
- Hence a transformed section would mean to a homogeneous concrete section.



Leavere arm

$$d = 460 - \frac{156}{3} = 408 \text{ mm}$$

Stress in steel (f_{st})

$$\frac{M}{A_{st} \times (d - \frac{x}{3})} = \frac{30 \times 10^6}{603 \times 408} = 121.93 \text{ N/mm}^2$$

Stress in concrete (f_{cb})

$$\frac{f_{st}}{m} \times \frac{x}{d - x}$$

$$= \frac{121.93}{13.33} \times \frac{156}{460 - 156}$$

$$= 4.7 \text{ N/mm}^2$$

Moment of Resistance (Comp)

$$M \cdot R = \frac{\sigma_{cbc} \cdot b \cdot x}{2} \times L \cdot A$$

$$= \frac{7 \times 200 \times 156}{2} \times 408 = 44553600 \text{ Nmm} \times 10^{-6}$$

$$= 44.5 \text{ kNm}$$

M.R in tension

$$\sigma_{st} \cdot A_{st} \cdot L \cdot A = 146 \times 603 \times 408 = 34443360 \text{ Nmm}$$

$$= 34.43 \text{ kNm}$$

Moment of Resistance of section = 34.43 kNm
(The smaller of the above two value)

have 3 no of 16 mm ϕ bar.

Given data :-

Width of beam (b) = 200 mm

Effective depth = 460 mm.

Moment = 30 kNm

For M20 grade Concrete σ_{cbc}
= 7 N/mm²

For Fe250 grade steel σ_{st} = 140 N/mm²

No of bar = 3

dia of bar = 16 mm.

$$A_{st} = 3 \times \frac{\pi}{4} \times 16^2 = 603 \text{ mm}^2$$

$$\text{Modular ratio} = \frac{280}{21} = 13.33 \text{ N/mm}^2$$

To find out min depth (x)

$$b \cdot x \cdot \frac{x}{2} = m A_{st} (d - x)$$

$$\Rightarrow 200 \times \frac{x^2}{2} = 13.33 \times 603 (460 - x)$$

$$\Rightarrow 100x^2 = 13.33 \times 603 (460 - x)$$

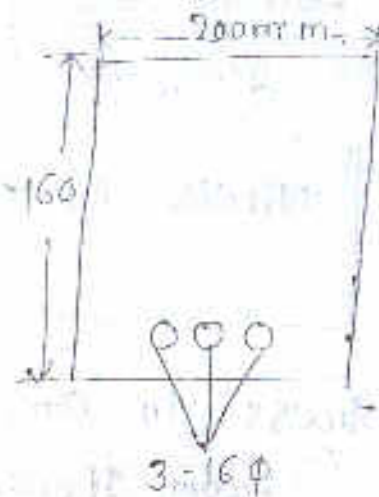
$$\Rightarrow 100x^2 = 8037 (460 - x)$$

$$\Rightarrow 100x^2 = 8037 \times 460 - 8037x$$

$$\Rightarrow 100x^2 = 3697020 - 8037x$$

$$\Rightarrow 100x^2 + 8037x - 3697020 = 0$$

$$\Rightarrow x = 156 \text{ mm}$$



25 A rectangular beam 200mm wide & 460mm effective depth having 3no of 16mm dia bar. The materials are M20 grade concrete & mild steel check whether the sec is balanced design, U/R design or R/D.

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Given data:-

$$\text{Width of beam} = 200\text{mm}$$

$$\text{effective depth} = 460\text{mm}$$

$$A_{st} = 3 \times \frac{\pi}{4} \times 16^2 = 603\text{mm}^2$$

$$m = \frac{280}{3 \times 7} = \frac{280}{21} = 13.33 \text{ N/mm}^2$$

$$\sigma_{cbc} = 7 \text{ N/mm}^2$$

$$\sigma_{st} = 140 \text{ N/mm}^2$$

To find out N/A depth (x)

$$b \alpha \cdot \frac{\alpha}{2} = m A_{st} (d - x)$$

$$200 \frac{\alpha^2}{2} = 13.33 \times 603 (460 - x)$$

$$\Rightarrow x = 156\text{mm}$$

To find balanced design N/A

$$x_{bal} = K_d d = 0.4 \times 460 = 184\text{mm}$$

$$x_{bal} = 184\text{mm}, \quad x = 156\text{mm}$$

$$x_{bal} > x$$

\(\therefore\) the section is under-reinforced section.

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Types of problem

In single reinforced beam, there are two types of problem.

- (1) Analysis of the section
- (2) Design of the section

Analysis of the section

Type - 1

To find out the depth of neutral axis for a given section & specifying the type of beam.

Step-1

If the section & actual stresses in the materials are given, find out the depth of neutral axis using

$$\text{equation } \boxed{N \cdot A = b \cdot x \cdot \frac{\sigma_c}{\sigma_s} = m A_s t (d - x)}$$

$$(ii) \quad \boxed{x_{\text{critical}}} \quad , \quad k = \frac{1}{1 + \frac{\sigma_s t}{m E_s c}}$$

(iii) If $x_{\text{actual}} < x_{\text{critical}}$, then the beam is under reinforced section.

(iv) If $x_{\text{actual}} = x_{\text{critical}}$, balance section

(v)

Type-2

To find the MR of the given section.

Step-1

- (i) Find the depth of NA.
- (ii) Find the depth of critical NA $x = kd$.
- (iii) If $x_{act} < x_{critical}$, the section is under reinforced section.

$$MR = A_s f_{st} (d - x/3)$$

- (iv) If $x_{act} > x_{critical}$, the section is over reinforced section.

$$MR = b \cdot x \frac{f_{cb}}{2} (d - x/3)$$

Type-3

For the given moment & section of beam to check the stresses.

- Q Determine the position of neutral axis of a reinforced concrete beam 200 mm wide & 400 mm effective depth if the stress developed in concrete & steel are 6.5 N/mm^2 & 212 N/mm^2 respectively. The materials are M20 grade concrete & HYSD reinforcement of grade Fe25. Also state the type of beam. Assume 4 no of 16 mm dia bar used.

Solⁿ

Given data:-

Width of the beam = 230 mm

Effective depth of beam (d) = 460 mm

no of bars = 4, dia = 16 mm

$$A_{st} = 4 \times \frac{\pi}{4} \times 16^2 \\ = 804.24 \text{ mm}^2$$

$$m = \frac{280}{3 \times 7} = \frac{280}{3 \times 7} = 13.33$$

For M20 grade concrete $\sigma_{cbc} = 7 \text{ N/mm}^2$

For HYSD bar Fe415, $\sigma_{st} = 230 \text{ N/mm}^2$

Step-1

To find out depth of neutral axis (actual)

$$bx \cdot \frac{x}{2} = m A_{st} (d - x)$$

$$\Rightarrow 230 \cdot \frac{x^2}{2} = 13.33 \times 804.24 (460 - x)$$

$$\Rightarrow 115x^2 = 10720.51 (460 - x)$$

$$\Rightarrow 115x^2 = 4931438.6 - 10720.51x$$

$$\Rightarrow 115x^2 + 10720.51x - 4931438.6 = 0$$

$$\Rightarrow x = 165.49 \text{ mm}$$

$$x_{act} = 165.5 \text{ mm}$$

Step-2

Critical N.A depth

$$x_{critical} = K_d$$

$$k = \frac{1}{1 + \frac{f_{st}}{6e_b c}}$$

$$= 0.29$$

$$x_{critical} = 0.29 \times 460$$

$$= 133.4 \text{ mm}$$

$$x_{act} = 165.5 \text{ mm}$$

$$x_{critical} = 133.4 \text{ mm}$$

$$x_{critical} < x_{actual}$$

So the beam is over reinforced section.

Step 3

M.R of the section

$$MR = \frac{1}{2} f_{cb} b \cdot x \cdot (d - \frac{x}{3})$$

$$= \frac{1}{2} \times 7 \times 230 \times 165.5 \left(460 - \frac{165.5}{3} \right)$$

$$= 61284594.83 \text{ Nmm}$$

$$= 61.28 \text{ kNm}$$

Q Find the MR of the beam as shown in figure. Also state whether the beam is U.R or O.R. The materials used M20 grade concrete & HYSD reinforcement.

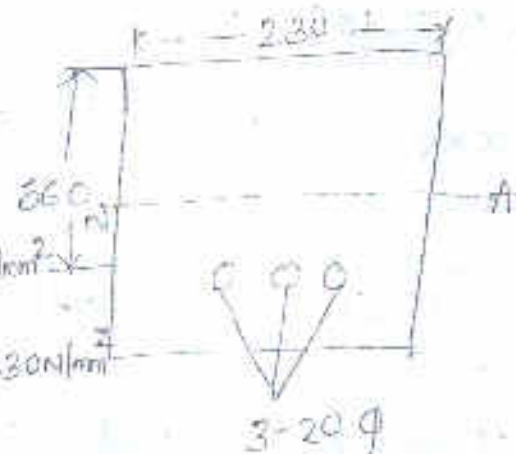
Given data :-

Materials used M20 grade concrete

HYSD bar Fe415

$$A_{st} = 3 \times \frac{\pi}{4} \times 20^2$$

$$= 942.47$$



Neutral depth axis (x_{actual})

$$b \cdot x \cdot \frac{\alpha}{2} = m A_s t (d - x)$$

$$230 \cdot \frac{x^2}{2} = 13.33 \times 942.47 \cdot (560 - x)$$

$$\Rightarrow 115x^2 = 12563.127 (560 - x)$$

$$\Rightarrow 115x^2 = 7035347.2 - 12563.127x$$

$$\Rightarrow 115x^2 + 12563.127x - 7035347.2 = 0$$

$$\Rightarrow x_{actual} = 198.67$$

$$K_d = 0.29 \times 560 = 162.4$$

$$x_{crit} = 198.6 \text{ mm}$$

$$x_{critical} = 162.4 \text{ mm}$$

$$x_{critical} < x_{actual}$$

So the beam is over-reinforced section.

Moment of Resistance

$$= \frac{1}{2} \sigma_{cbc} \cdot b \cdot x (d - \frac{x}{3})$$

$$= \frac{1}{2} \times 7 \times 230 \times 198.6 \left(560 - \frac{198.6}{3} \right)$$

$$= 89528813.8 \text{ Nmm} = 78945287 \text{ Nmm}$$

$$= 78.94 \text{ kN}$$

Q A simply supported beam of size $230\text{mm} \times 600\text{mm}$ overall depth is reinforced with 4 no of 12mm dia bar. Find the safe load on the beam in addition to its self wt on a span of 4m . The materials are M20 grade concrete & HYSD reinforcement of Fe 415.

Given data :-

Overall depth (D) = 600mm

Width of beam (b) = 230mm

No of bars = 4, dia = 12mm

Area of steel (A_{st})

$$= 4 \times \frac{\pi}{4} \times 12^2$$

$$= 452.38\text{mm}^2$$

M20 grade conc. $\sigma_{cbc} = 7\text{N/mm}^2$

HYSD reinforcement, $\sigma_{st} = 230\text{N/mm}^2$

Neutral axis depth

Assume $c_c = 30\text{mm}$

$$d = 600 - 30 - 6 = 564\text{mm}$$

Neutral axis depth x_{actual}

$$b \times \frac{x}{3} = M_{AST} (d - x)$$

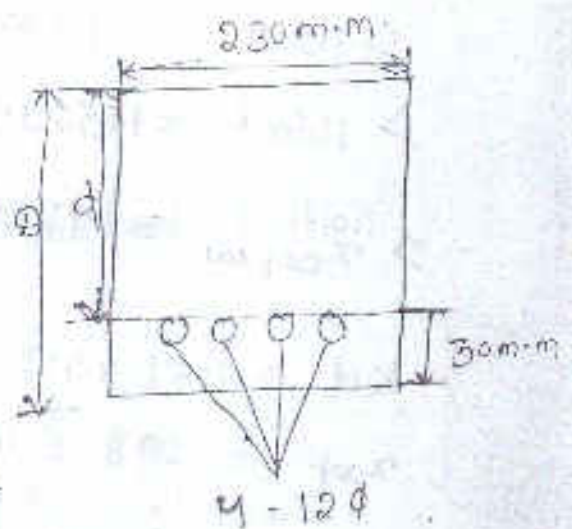
$$\Rightarrow 230 \frac{x^2}{3} = 13.33 \times 452 (564 - x)$$

$$\Rightarrow 115x^2 = 6025.16 (564 - x)$$

$$\Rightarrow 115x^2 = 3398190.24 - 6025.16x$$

$$\Rightarrow 115x^2 + 6025.16x - 3398190.24 = 0$$

$$\Rightarrow x_{act} = 147.7$$



Critical depth of n.A (critical)

35

$$x_{critical} = k \times d$$

$$= 0.29 \times 564$$

$$= 163.56 \text{ mm}$$

$x_{act} < x_{critical}$, So the beam is under reinforced section.

Moment of Resistance

$$M_R = A_{st} \sigma_{st} (d - x/3)$$

$$\Rightarrow M_R = 452 \times 230$$

$$= 53.51 \text{ kNm}$$

Let the load on beam = w kNm

$$M = \frac{wl^2}{8} = \frac{w \times 4^2}{8}$$

$$= \frac{w \times 4^2}{8} \times 53.51$$

$$w = \frac{53.51 \cdot 8}{4^2} = 26.76 \text{ kNm}$$

$$\text{Self wt of the beam} = 0.23 \times 0.6 \times 25$$
$$= 3.45 \text{ kNm}$$

$$\text{Safe load} = 26.7 - 3.45 = 23.25$$

Q.3 A simply supported beam over a span of 4.5m is reinforced with tension reinforcement only. The beam is 250mm wide and has an effective depth of 610mm. It is reinforced with 4 no 20mm dia bars. Calculate the stresses in both the materials at the center of the span when the beam carries a uniformly distributed load of 30 kN/m inclusive of self weight. The materials are M20 grade concrete and HYSD reinforcement of grade Fe415.

Sol Given data :-

Width of beam (b) = 250mm

effective depth (d) = 610mm

4 no of bar dia 20mm moment (M) = $\frac{wl^2}{8} = \frac{30 \times 4.5^2}{8}$

$A_{st} = 4 \times \frac{\pi}{4} \times 20^2 = 1256.6 \text{ mm}^2$

$= 1256.6 \text{ mm}^2$

M20 grade concrete $f_{cbc} = 7 \text{ N/mm}^2$

HYSD reinforcement $f_{st} = 230 \text{ N/mm}^2$

modular ratio:-
 $(m) = \frac{280}{3 \times f_{cbc}} = \frac{280}{3 \times 7} = 13.33$

Step 1
Neutral axis depth (x)

$$b \cdot x \cdot \frac{x}{2} = m A_{st} (d - x)$$

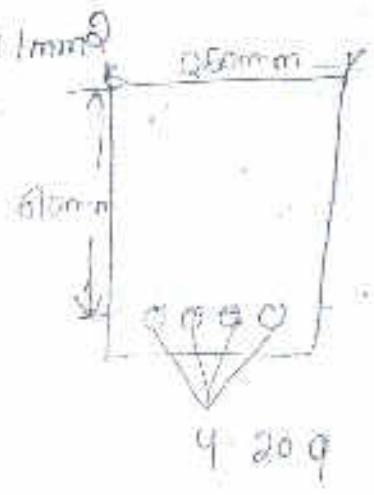
$$\Rightarrow 250 \cdot \frac{x^2}{2} = 13.33 \times 1256 (610 - x)$$

$$\Rightarrow 125x^2 = 16742.48 (610 - x)$$

$$\Rightarrow 125x^2 = 10212912.8 - 16742.48x$$

$$\Rightarrow 125x^2 + 16742.48x - 10212912.8 = 0$$

$$x_{act} = 226.6$$



critical neutral axis depth (neutral)

$$x_{critical} = \frac{M}{f_y A_s}$$

$$= \frac{75.93 \times 10^6}{13.33 \times 610}$$

Step 2

$$\text{Stress in steel } F_{st} = \frac{M}{A_s (d - x/3)}$$

$$= \frac{75.93 \times 10^6}{1256 \left(610 - \frac{226.6}{3}\right)} = 113.11 \text{ N/mm}^2$$

Stress in concrete (F_{cb})

$$\frac{F_{st}}{M} \times \frac{x}{d-x} = \frac{113.11}{13.33} \times \frac{226.6}{610 - 226.6}$$

$$= 5.01 \text{ N/mm}^2$$

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Q10 A rectangular beam 230 mm wide x 580 mm effective depth is reinforced with 3 no of 16 mm dia bars calculate the stress in both the materials when a bending moment of 50 kNm is applied. The materials are M20 grade concrete & HYSD reinforcement. Also calculate MR of the section.

Solⁿ Given data
width of beam = 230 mm.

effective depth (d) = 560 mm.

$$A_{st} = 3 \times \frac{\pi}{4} \times 16^2 = 603.18 \text{ mm}^2$$

M20 grade concrete $f_{cbc} = 7 \text{ N/mm}^2$

HYSD reinforcement $f_{st} = 236 \text{ N/mm}^2$

$$M = 50 \text{ kNm}$$

$$m = \frac{280}{3 \times 7} = 13.33$$

Step - 1

To find out N.A depth (x)

$$b \cdot x \cdot \frac{x}{2} = m A_{st} (d - x)$$

$$230 \cdot \frac{x^2}{2} = 13.33 \times 603.18 (560 - x)$$

$$\Rightarrow 115x^2 = 13.33 \times 603.18 (560 - x)$$

$$\Rightarrow 115x^2 = 8037.99 (560 - x)$$

$$\Rightarrow 115x^2 = 4501274.4 - 8037.99x = 0$$

$$\Rightarrow 115x^2 + 8037.99x - 4501274.4 = 0$$

$$\Rightarrow x = 165.9$$

Step - 2

$$\text{Stress in steel } (f_{st}) = \frac{M}{A_{st} (d - x/3)}$$

$$= \frac{50 \times 10^6}{603.18 \times (560 - \frac{165.9}{3})}$$

$$= 164.2 \text{ N/mm}^2$$

$$\text{Stress in concrete } (f_{cb}) = \frac{F_{st}}{m} \times \frac{x}{d-x}$$

$$= \frac{164.29}{13.33} \times \frac{165.95}{560 - 165.95}$$

$$= 5.19 \text{ N/mm}^2$$

$$\frac{\alpha_{critical}}{\alpha} = kd$$

$$= 0.29 \times 560 = 162.4 \text{ mm}$$

$$165 \text{ mm} > \alpha_{critical}$$

\therefore The beam is over reinforced section.

$$\text{So, } MR = \frac{\sigma_{cbc} \cdot b \cdot x}{2} \times d - \frac{x}{3}$$

$$= \frac{7 \times 230 \times 165}{2} \times 560 - \frac{165}{3}$$

$$= 67.43 \text{ kNm}$$

Q A simply supported beam of 6m span carries a u.d.l of 12 kN/m inclusive of self wt. The beam 230 mm wide & the effective depth is 580 mm. Find the steel area, the materials are M20 grade conc. & HYSD reinforcement.

Given data:-

$$\text{width of beam} = 230 \text{ mm}$$

$$\text{Effective depth } (d) = 580 \text{ mm}$$

$$\text{u.d.l} = 12 \text{ kN/m}$$

span length (L) = 6m

M20 grade concrete $f_{ck} = 20 \text{ N/mm}^2$

HYSD reinforcement $f_{st} = 230 \text{ N/mm}^2$

step-1

$$M = \frac{wl^2}{8} = \frac{12 \times 6^2}{8} = 54 \text{ kNm}$$

$$\text{depth reqd} = \sqrt{\frac{M}{R_{bal} \times b}}$$

$$\sqrt{\frac{54 \times 10^6}{0.91 \times 230}} = 507 \text{ mm}$$

Actual depth = 580 mm

depth reqd = 507 mm

$$580 > 507$$

The beam is under reinforced section.

$$M \cdot R = f_{st} A_{st} (d - \alpha/3)$$

$$= 230 \times A_{st} (580 - \alpha/3)$$

$$M = mR$$

$$\Rightarrow 54 \times 10^6 = 230 A_{st} (580 - \alpha/3)$$

$$\Rightarrow \frac{54 \times 10^6}{230} = A_{st} (580 - \alpha/3)$$

$$\Rightarrow 234782.60 = A_{st} (580 - \alpha/3) \quad \text{--- (1)}$$

step - 2

To find depth of N.A

$$b \times \frac{x}{3} = m \text{ Ast } (d-x)$$

$$\Rightarrow 230 \frac{x^2}{3} = 13.33 \text{ Ast } (580-x)$$

$$\Rightarrow 115x^2 = 13.33 \text{ Ast } (580-x)$$

$$\Rightarrow \frac{115x^2}{13.33} = \text{Ast } (580-x)$$

$$\Rightarrow \text{Ast} = \frac{8.627}{580-x}$$

substituting in eqⁿ (i)

$$234782.60 = \text{Ast} \times (580 - \frac{x}{3})$$

$$\Rightarrow 234782.60 = \text{Ast} \left(\frac{1740-x}{3} \right)$$

$$\Rightarrow 234782.60 = \left(\frac{8.627x^2}{580-x} \right) \times \left(\frac{1740-x}{3} \right)$$

$$\Rightarrow 234782.60 = \left(\frac{8.627x^2}{580-x} \right) \times \left(\frac{1740-x}{3} \right)$$

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or

$$mR = 6st \text{ Ast } (d-x/3)$$

$$54 \times 10^6 = 230 \times \text{Ast} (d-x/3)$$

$$\Rightarrow 54 \times 10^6 = 230 \text{ Ast} \left(\frac{3d-x}{3} \right)$$

$$\Rightarrow 54 \times 10^6 = 76.66 \text{ Ast} (3d-x)$$

$$\Rightarrow \frac{54 \times 10^6}{76.66} = \text{Ast} (3d-x)$$

$$\frac{7070000}{76.66} = \text{Ast} (3d-x) \dots \dots \dots (ii)$$

Depth of N.A (x)

$$b \cdot x \cdot \frac{x}{2} = \text{MAST} (d-x)$$

$$230 \frac{x^2}{2} = 13.33 \text{ ASt} (d-x)$$

$$\Rightarrow \frac{115x^2}{13.33} = \text{ASt} (d-x)$$

$$\Rightarrow 8.63 x^2 = \text{ASt} (d-x)$$

$$\Rightarrow \text{ASt} = \frac{8.63 x^2}{d-x} \quad \text{--- (ii)}$$

Substituting in eqn (i)

$$\Rightarrow 704409.07 = \text{ASt} (3d-x)$$

$$\Rightarrow 704409.07 = \frac{8.63x^2}{d-x} \times (3d-x)$$

$$\Rightarrow 704409.07 = \frac{8.63x^2}{580-x} \times (3 \times 580 - x)$$

$$\Rightarrow 704409.07 = \frac{8.63x^2}{580-x} \times (1740 - x)$$

$$704409.07 \times (580-x) = (8.63x^2) (1740-x)$$

$$\Rightarrow 408557260.6 - 704409.07x = 15016.2x^2 - 8.63x^3$$

$$\Rightarrow 8.63x^3 - 15016.2x^2 - 704409.07x + 408557260.6 = 0$$

$$\Rightarrow x = 149 \text{ mm}$$

$$\text{ASt} = \frac{8.63x^2}{d-x} = \frac{8.63 \times 149^2}{580 - 149} = 444.32 \text{ mm}^2$$

Q A simply supported beam 250mm width & 610 overall depth is reinforced with 4no of 20mm dia bars. find out the depth of N.A & state what type of secⁿ. Also determine the M.R.

Given data:-

width of beam (b) = 250mm

overall depth (D) = 610mm

d = effective cover = 610 - 40 = 570mm

4 no of 20mm dia bars

$$A_{st} = 4 \times \frac{\pi}{4} \times 20^2 = 1256 \text{ mm}^2$$

M20 grade concrete = 7N/mm²

HYSD reinforcement $\sigma_{st} = 230 \text{ N/mm}^2$

To find out N.A (neutral)

$$b \cdot x \cdot \frac{x}{2} = m A_{st} (d - x)$$

$$\Rightarrow 250 \cdot \frac{x^2}{2} = 13.33 \times 1256 (570 - x)$$

$$\Rightarrow 125x^2 = 16742.48 (570 - x)$$

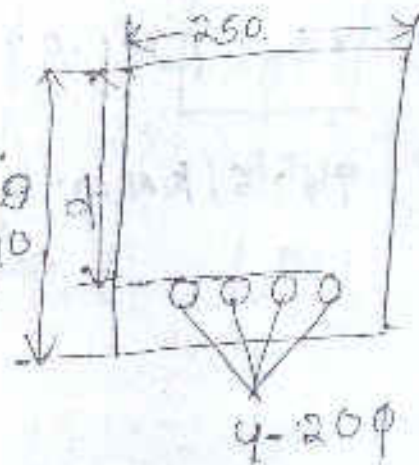
$$\Rightarrow 125x^2 = 9543213.6 - 16742.48x$$

$$\Rightarrow 125x^2 + 16742.48x - 9543213.6$$

$$\Rightarrow x_{act} = 217.33$$

$$x_{critical} = Kd$$

$$= 0.29 \times 217.33 = 63.03$$



So it is overreinforced section.

Moment of Resistance

$$\frac{1}{2} \sigma_{cbc} \cdot b \cdot x \left(d - \frac{x}{3} \right)$$

$$\Rightarrow \frac{1}{2} \times 7 \times 250 \times 217 \cdot 33 \times \left(570 - \frac{217 \cdot 33}{3} \right)$$

$$\Rightarrow 94617241.57 \text{ Nmm}$$

$$\Rightarrow 94.61 \text{ kNm}$$

Ans

18 May 2021

Doubly reinforced beam :-

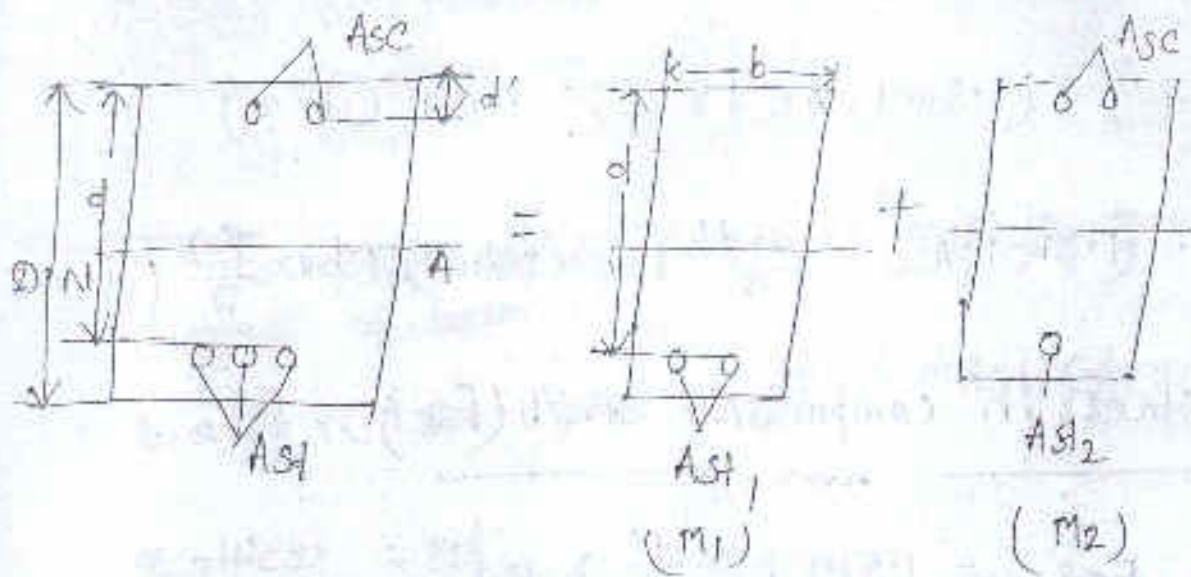
→ For a design moment M , if the size of the rectangular beam section is fixed & the moment of resistance of a singly reinforced section is less than M .

→ There are two methods to design such beams.

(i) Increase the concrete mix to increase the capacity of the section.

(ii) Reinforcement are provided in compression zone to give additional strength to the concrete in compression. Such

beams are called doubly reinforced beam.



$$(Moment) M = M_1 + M_2$$

$$M_2 = (1.5m - 1) A_{sc} \sigma_{cbc} \left(\frac{x - d'}{x} \right) x (d - d')$$

modular ratio

$$A_{st} = A_{st1} + A_{st2}$$

$$A_{sc} = \frac{M_2}{(1.5m - 1) \sigma_{cbc} \left(\frac{x - d'}{x} \right) (d - d')}$$

$$A_{st2} = \frac{M_2}{\sigma_{st} (d - d')}$$

$$A_{st1} = \frac{M_1}{\sigma_{st} j d}$$

* To find out depth of N.A

$$b \times \frac{x}{2} + (1.5m-1) A_{sc} (x-d') = m A_{st} (d-x)$$

$$M = (1.5m-1) A_{sc} \times \frac{x-d'}{x} f_{cb} \times (d-d') + b \times \frac{f_{cb}}{2} (d-x/3)$$

* Stress in compression steel (f_{sc})

$$F_{sc} = 1.5m \left(\frac{x-d'}{x} \right) f_{cb}$$

* Stress in tensile steel (f_{st})

$$F_{st} = m f_{cb} \left(\frac{d-x}{x} \right)$$

* Find moment of inertia section

$$I_x = \frac{1}{3} b x^3 + (1.5m-1) \times A_{sc} (x-d')^2 + m A_{st} (d-x)^2$$

$$\text{stress in concrete } (f_{cb}) = \frac{M \cdot x}{I_x}$$

$$F_{sc} = 1.5m \times \frac{M(x-d')}{I_x}$$

$$F_{st} = m \times \frac{M(d-x)}{I_x}$$

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Types of problems

Type - 1

To find out the depth of N.A & specify type of beam.

$$b \cdot x \cdot \frac{x}{2} + (1.5m - 1) A_{sc} (x - d') = m A_{st} (d - x)$$

$$x_{critical} = kd'$$

(a) If $x_{actual} < x_{critical}$, then the beam is under reinforced section.

(b) If $x_{act} > x_{critical}$, then the beam is over reinforced section.

Type - 2

For given moment & section of beam to check the stresses.

Type - 3

To find out the moment of resistance of the section.

(a) $x_{act} > x_{critical}$, over reinforcement

$$M \cdot R = M_1 + M_2 \\ = \frac{1}{2} \sigma_{cbc} b \cdot x (d - x/3) + (1.5m - 1) A_{sc} \sigma_{cbc} x \left(\frac{x - d'}{x} \right) (d - d')$$

(b) If $x_{act} < x_{critical}$, under reinforcement

$$M \cdot R = A_{st} \sigma_{st} (d - y)$$

$$\bar{y} = \frac{c_1 y_1 + c_2 y_2}{c_1 + c_2}$$

$$y_2 = d'$$

$$c_1 = \frac{bx}{2} f_{cb} \quad , \quad y_1 = \frac{x}{3}$$

$$c_2 = (1.5m-1) A_{sc} \left(\frac{x-d'}{x} \right) f_{cb}$$

(or)

M.R (Compression)

$$\frac{\sigma_{cbc} \times I_x}{x}$$

M.R (Tension)

$$\frac{\sigma_{st} \times I_x}{m(d-x)}$$

Type - 4 : To design the section

(a) Find $M_1 = Qbd^2$

(b) If $M > M_1$, design as doubly reinforced beam.

(c) Find $A_{st1} = \frac{M_1}{\sigma_{st} j d}$, $A_{st2} = \frac{M_2}{\sigma_{st} (d-d')}$

$$A_{st} = A_{st1} + A_{st2}$$

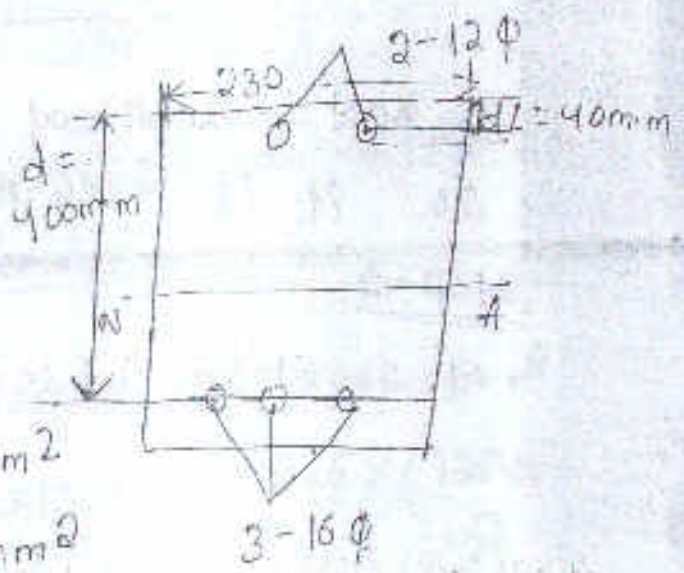
$$A_{sc} = \frac{M_2}{(1.5m-1)\sigma_{cbc} \left(\frac{x-d'}{x}\right)(d-d')}$$

Depth of N.A, type of beam, stress, MR

16 A rectangular beam is reinforced as shown in Fig. Find out the maximum stress in concrete & steel. If it is subjected to a moment 40 kNm. The materials are M20 grade concrete & HYSD reinforcement. Also find out MR of the section.

Given data:-

- width of beam (b) = 230 mm
- Effective depth (d) = 400 mm
- d' = 40 mm



$$A_{sc} = 2 \times \frac{\pi}{4} \times 12^2 = 226 \text{ mm}^2$$

$$A_{st} = 3 \times \frac{\pi}{4} \times 16^2 = 603 \text{ mm}^2$$

For M20 grade concrete $\sigma_{cbc} = 7 \text{ N/mm}^2$

HYSD steel $\sigma_{st} = 230 \text{ N/mm}^2$

$$m = \frac{280}{3 \times 7} = 13.33$$

Step 1

To find out depth of N.A

$$b \cdot x \cdot \frac{x}{2} + (1.5m-1)A_{sc}(x-d') = m A_{st} \cdot (d-x)$$

$$230 \frac{x^2}{2} + (1.5 \times 13.33 - 1) 226 (x - 40) = 13.33 \times 603 (400 - x)$$

$$\Rightarrow 115x^2 + 4292.87x(x-40) = 8037.99(400-x)$$

$$\Rightarrow 115x^2 + 4292.87x - 171714.8 = 3215196 - 8037.99x$$

$$\Rightarrow 115x^2 + 4292.87x + 8037.99x - 171714.8 + 3215196 = 0$$

$$\Rightarrow 115x^2 + 12330.86x - 3386910.8 = 0$$

$$x = 126.18 \text{ m.m.}$$

$$x_{\text{critical}} = kd$$

$$k = 0.29$$

$$= 0.29 \times 400 = 116 \text{ m.m.}$$

$$x_{\text{act}} > x_{\text{critical}}$$

so it is over reinforced section.

step-2

$$M = (1.5m-1) A_s c \left(\frac{x-d'}{x} \right) f_{cb} (d-d') + b x \times \frac{f_{cb}}{2} \left(d - \frac{x}{3} \right)$$

$$42 \times 10^6 = (1.5 \times 13.33 - 1) 226 \left(\frac{126.18 - 40}{126.18} \right) f_{cb} (400 - 40)$$

$$+ 230 \times 126.18 \times \frac{f_{cb}}{2}$$

$$\left(400 - \frac{126.18}{3} \right)$$

$$\Rightarrow 42 \times 10^6 = 2931.99 \times 360 f_{cb} + 29021.4 \times \frac{f_{cb}}{2} \times 257.94$$

$$\Rightarrow 42 \times 10^6 = 1055516.4 f_{cb} + 5193959.95$$

$$\Rightarrow 42 \times 10^6 = 6249476.35 f_{cb}$$

$$f_{cb} = \frac{42 \times 10^6}{6249476.35} = 6.72 \text{ N/mm}^2$$

stress in steel in compression

$$f_{sc} = 1.5m \left(\frac{x-d'}{x} \right) f_{cb}$$

$$= 1.5 \times 13.33 \left(\frac{126.18 - 40}{126.18} \right) \times 6.72$$

$$= 91.77 \text{ N/mm}^2$$

stress in steel in tension

$$f_{st} = m f_{cb} \left(\frac{d-x}{x} \right)$$

$$= 13.33 \times 6.72 \times \left(\frac{400 - 126.18}{126.18} \right)$$

$$f_{st} = 194.39 \text{ N/mm}^2$$

(or)

$$I_x = \frac{1}{3} b x^3 + (1.5m-1) A_{sc} (x-d')^2 + m a s t (d-x)^2$$

$$= \frac{1}{3} \times 230 \times 126.18^3 + (1.5 \times 13.33 - 1) \times 226 \times (126.18 - 40)^2$$

$$+ 13.33 \times 603 (400 - 126.18)^2$$

$$= 788571009 \text{ N/mm}^2$$

$$f_{cb} = \frac{M \cdot x}{I_x} = \frac{42 \times 10^6 \times 126.18}{788571009} = 6.72 \text{ N/mm}^2$$

$$f_{sc} = 1.5m \times \frac{m(x-d')}{I_x} = \frac{1.5 \times 13.33 \times \frac{40 \times 10^6}{126.18}}{788571009}$$

$$= 91.8 \text{ N/mm}^2$$

$$F_{st} = m \times \frac{M(d-x)}{I_x}$$

$$= \frac{13.33 \times 40 \times 10^6 (400 - 126.18)}{188571009}$$

$$= 194 \text{ N/mm}^2$$

Step-3

$$M \cdot R = M_1 + M_2$$

$$= \frac{1}{2} \sigma_{cbc} \cdot b \cdot x (d - x/3) + (1.5m - 1) A_{sc} \sigma_{cbc} x \left(\frac{x - d'}{x} \right) (d - d')$$

$$= \frac{1}{2} \times 7 \times 230 \times 126.18 \times \left(400 - \frac{126.18}{3} \right) + 1.5 \times (13.33 - 1) \times 226 \times 7 \times \frac{126.18 - 40}{126.18} (400 - 40)$$

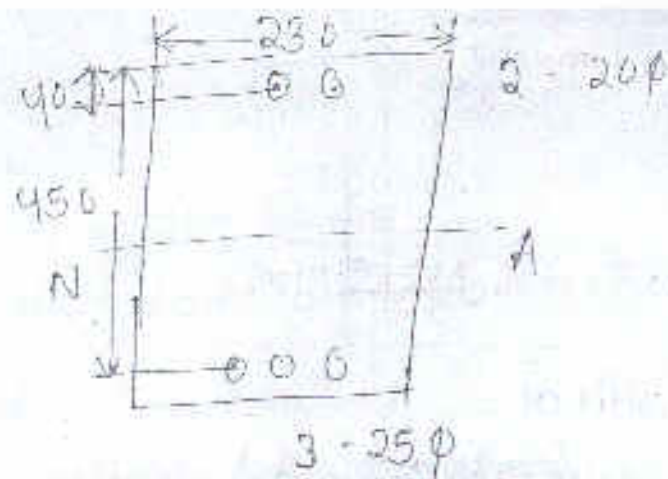
$$= 43746355.24 \text{ Nmm}$$

$$= 43.74 \text{ kNm}$$

21 May 2021

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A rectangular beam is reinforced as shown in fig. Find out the M.R of the section. The materials are M20 grade concrete & HYSD reinforcement of grade Fe 415.



Given data :-

width of the beam = 230 mm

$d' = 40 \text{ mm}$

Effective depth = 450 mm

$$A_{sc} = 2 \times \frac{\pi}{4} \times 20^2 = 628 \text{ mm}^2$$

$$A_{st} = 3 \times \frac{\pi}{4} \times 25^2 = 1472 \text{ mm}^2$$

For M20 grade concrete $f_{ck} = 20 \text{ N/mm}^2$

HYSD steel $f_{yk} = 235 \text{ N/mm}^2$

$$m = \frac{280}{3 \times 7} = 13.33$$

Step-1

to find out x

$$b \cdot x \cdot \frac{x}{2} + (1.5m - 1) A_{sc} (x - d') = m A_{st} (d - x)$$

$$\Rightarrow 230 \frac{x^2}{2} + (1.5 \times 13.33 - 1) 628.31 (x - 40) = 13.33 \times 1472.62 (450 - x)$$

$$\Rightarrow 115x^2 + 11934.74(x - 40) = 19630.02(450 - x)$$

$$\Rightarrow 115x^2 + 11934.74x - 477389.6 = 883350.91 - 19630.02x$$

$$\Rightarrow 11x^2 + 31564.76x - 9310898.6 = 0$$

$$x_1 = 178.67 \text{ mm}$$

Kol

$$0.29 \times 450 = 130.5 \text{ mm}$$

$x_{act} > x_{critical}$

So it is over reinforced section.

Step-2

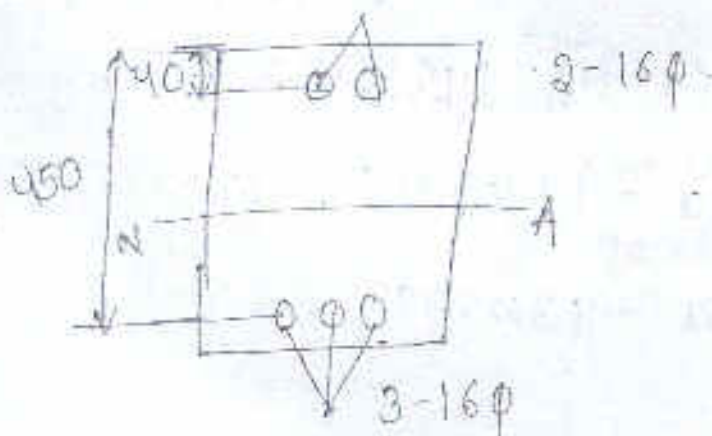
M.R

$$\frac{1}{2} \times 7 \times 230 \times 178.67 \times \left(450 - \frac{178.67}{3} \right) + (1.5 \times 13.33 - 1) \times 628.31 \times 7 \times \left(\frac{178.67 - 40}{178.67} \right) (450 - 40)$$

$$= 82741560.76 \text{ Nmm}$$

$$= 82.74 \text{ kNm}$$

3Q A rectangular beam is reinforced as shown in fig. find out the MR of the section. The materials are M20 grade conc. & mild steel reinforcement.



22 May 2021

Given data:-

width of beam (b) = 230 mm.

Effective depth (d) = 450 mm

d' = 40 mm.

$$A_{sc} = 2 \times \frac{\pi}{4} \times 16^2 = 402.12 \text{ mm}^2$$

$$A_{st} = 3 \times \frac{\pi}{4} \times 16^2 = 603 \text{ mm}^2$$

M20 grade concrete $\sigma_{cbc} = 7 \text{ N/mm}^2$

mild steel $\sigma_{st} = 140 \text{ N/mm}^2$

$$m = \frac{280}{3 \times 7} = 13.33$$

Step 1.

to find out x_{ae}

$$b \cdot x \cdot \frac{x}{2} + (1.5m - 1) A_{sc} (x - d') = m A_{st} (d - x)$$

$$\Rightarrow 230 \frac{x^2}{2} + (1.5 \times 13.33 - 1) 402 (x - 40) = 13.33 \times 603 (450 - x)$$

$$\Rightarrow 115x^2 + 7635.99 (x - 40) = 8037.99 (450 - x)$$

$$\Rightarrow 115x^2 + 7635.99x - 305439.6 = 8037.99 \cdot 3617095.5 - 8037.99x$$

$$\Rightarrow 115x^2 + 15673.98 - 3922535.1 = 0$$

$$x_{ae} = 128 \text{ mm}.$$

$$x_{critical} = k_{ed} = 0.9 \times 450 = 180 \text{ mm}.$$

$x_{ed} < x_{critical}$ so the beam is in under reinforced section.

$$MR = A_{st} \sigma_{st} (d - \bar{y})$$

$$C_1 = \frac{b x}{2} f_{cb} = \frac{230 \times 128}{2} f_{cb} = 14720 f_{cb}$$

$$C_2 = (1.5m - 1) A_{sc} \left(\frac{x - d'}{x} \right) f_{cb}$$
$$= (1.5 \times 13.33 - 1) 402 \left(\frac{128 - 40}{128} \right) f_{cb}$$

$$= 5249.74 f_{cb}$$

$$y_1 = \frac{128}{3} = 42.67$$

$$y_2 = 40 \text{ m.m.}$$

$$\bar{y} = \frac{C_1 y_1 + C_2 y_2}{C_1 + C_2} = \frac{14720 f_{cb} \times 42.67 + 5249.74 f_{cb} \times 40}{14720 f_{cb} + 5249.74 f_{cb}}$$

$$= \frac{628102.4 f_{cb} + 209989.6 f_{cb}}{19969.74 f_{cb}}$$

$$= 41.96 \text{ m.m.}$$

$$MR = A_{st} \sigma_{st} (d - \bar{y})$$

$$= 603 \times 140 (450 - 41.96)$$

$$= 34 \text{ kNm}$$

(OR)

$$MR (\text{comp}) = \frac{\sigma_{cbc} I_x}{x} = \frac{57501173.76}{14} = 51 \text{ kNm}$$

$$MR (\text{tension}) = \frac{\sigma_{st} I_x}{m(d-x)} = 34 \text{ kNm}$$

24 May 2021

15

A rectangular cantilever beam of size 230 mm width \times 500 mm effective depth is subjected to a bending moment of 80 kNm. Design the reinforcement for flexure. The materials are M20 grade concrete & HYSD reinforcement.

Given data:-

Width of beam (b) = 230 mm

Effective depth (d) = 500 mm

Bending moment (M) = 80 kNm

M20 grade σ_{cbc} = 7 N/mm²

HYSD reinforcement σ_{st} = 230 mm

step-1

$$\begin{aligned} M_1 &= \sigma_{cbc} \times b d^2 \\ &= 0.91 \times 230 \times 500^2 \\ &= 52.33 \text{ kNm} \end{aligned}$$

$M > M_1$ so the beam is doubly reinforced - cement

$$\begin{aligned} A_{st1} &= \frac{M_1}{\sigma_{st} j d} \\ &= \frac{52.33}{230 \times 0.4 \times 500} = 506 \text{ mm}^2 \end{aligned}$$

$$M = M_1 + M_2$$

$$M_2 = M - M_1 = 80 - 52.33 = 27.67 \text{ kNm}$$

$$m = \frac{280}{1.15} = 13.33$$

$$A_{sc} = \frac{M_2}{(1.5m-1) \sigma_{cbc} \left(\frac{x-d'}{x}\right) (x-d')}$$

$$= \frac{27.67 \times 10^6}{(1.5 \times 13.33 - 1) 7}$$

$$= 624.73 \text{ mm}^2 \approx 625 \text{ mm}^2$$

$$A_{st2} = \frac{M_2}{\sigma_{st} (d-d')} = \frac{27.67 \times 10^6}{230 (500-40)}$$

$$= 261.53 \approx 262 \text{ mm}^2$$

Assume $d' = 40 \text{ mm}$.

$$A_{st} = A_{st1} + A_{st2} = 506 + 262 = 768 \text{ mm}^2$$

$$A_{sc} = 625 \text{ mm}^2$$

Assume provide 3 no of 20 mm dia bars at top as compression zone.

$$A_{sc} = 3 \times \frac{\pi}{4} \times 20^2 = 942 \text{ mm}^2$$

provide 4 no of 16 mm at bottom of beam

$$A_{st} = 4 \times \frac{\pi}{4} \times 16^2 = 804 \text{ mm}^2$$

Step-2

To find neutral axis depth

$$b \cdot x \cdot \frac{x}{2} + (1.5m-1) A_{sc} (x-d') = m A_{st} (x-x')$$

$$= 230 \frac{x^2}{2} + (1.5 \times 13.33) 942 (x-40) = 13.33 \times 804 (500-x)$$

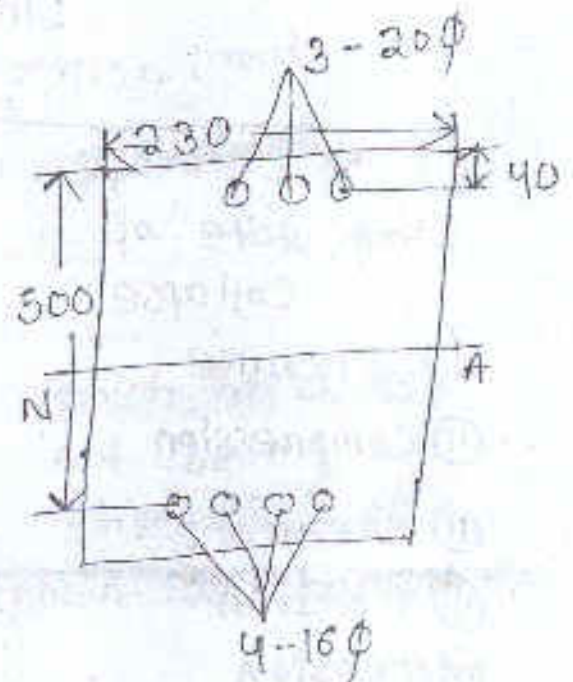
$$i \Rightarrow 115x^2 + 17893.29(x-40) = 10717.32(500-x)$$

$$\Rightarrow 115x^2 + 17893.29x - 715731.6 = 5358660 +$$

$$10717.32x$$

$$\Rightarrow 115x^2 + 28610.61x - 6074391.6$$

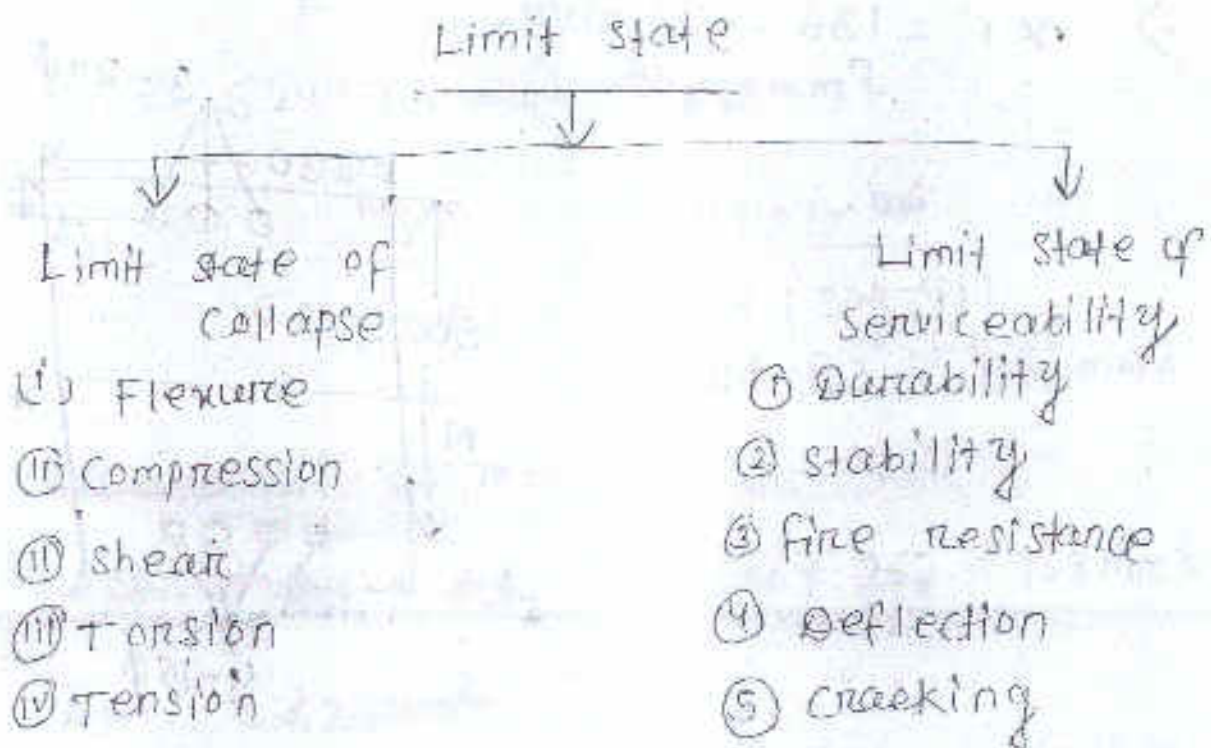
$$\Rightarrow x_1 = 136.93 \text{ mm.}$$



Limit state design

25 May 2021

The acceptable limit for the safety & serviceability requirements before failure occurs is called as limit state method.



Limit state design

The accept. characteristic strength of materials

The characteristic strength of materials is that value of the strength of the material below which not more than 5% of the test results are expected to fail.

Grade of conc.

Characteristic strength (Fck)

M15	→	15 N/mm ²
M20	→	20 N/mm ²
M25	→	25 N/mm ²

M30 \longrightarrow 30 N/mm²

M35 \longrightarrow 35 N/mm²

Grade of steel

characteristic strength (F_y)

Fe250 \longrightarrow F_y = 250 N/mm²

Fe415 \longrightarrow F_y = 415 N/mm²

Fe500 \longrightarrow F_y = 500 N/mm²

Characteristic Load

The value of load which has a 95% of probability of not being exceeded during the life of the structure is known as characteristic load.

31 May 2021

Partial safety factors :-

Types of Load

Dead Load

Live Load

wind Load

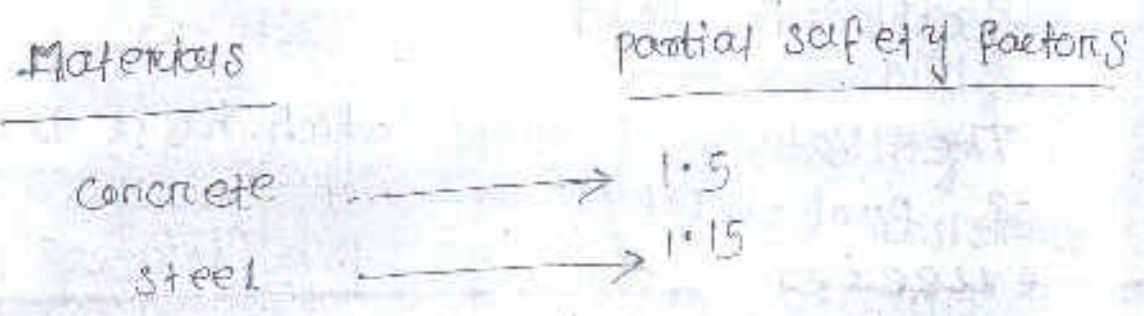
Earthquake Load

Impact Load

snow Load

Load Combination	Limit state of collapse			Limit state of serviceability		
	DL	LL	WL	DL	LL	WL
DL + LL	1.5	1.5		1.0	1.0	
DL + WL	1.5		1.5	1.0		1.0
DL + LL + WL	1.2	1.2	1.2	1.0	0.8	0.8

Partial safety factor (γ_m) for materials :-
 _____ 0 0 0 0 0 _____ 0 0 0 _____



Limit state of collapse :- Flexure :-
 _____ 0 0 0 0 0 0 0 _____

Assumptions

- ① plane section normal to the axis remain plane after to the bending.
- This assumption means that strain at any point on the cross section is directly proportional to its distance from the neutral axis.
- ② The maximum strain in concrete at the outermost compression fibre is taken as 0.0035 in bending.
- ③ The stress - strain diagram of concrete is parabolic from strain value of zero to ϵ_{max} & corresponding stress value of zero.

The stress now remains constant & strain increase to 0.0025. The relationship between the compressive stress distribution in concrete & the strain in concrete may be assumed to be rectangular, trapezoid, parabola or any other shape for design purposes. The compressive strength of concrete in the structure shall be assumed to be 0.67 times the characteristic strength.

- ④ The tensile strength of concrete is ignored.
- ⑤ The stresses in reinforcement are derived from representative stress-strain curve for the type of steel used.
- ⑥ The maximum strain in the tension reinforcement in the section at failure shall not be less than

$$E_s = \frac{F_y}{1.15 E_s} + 0.002$$

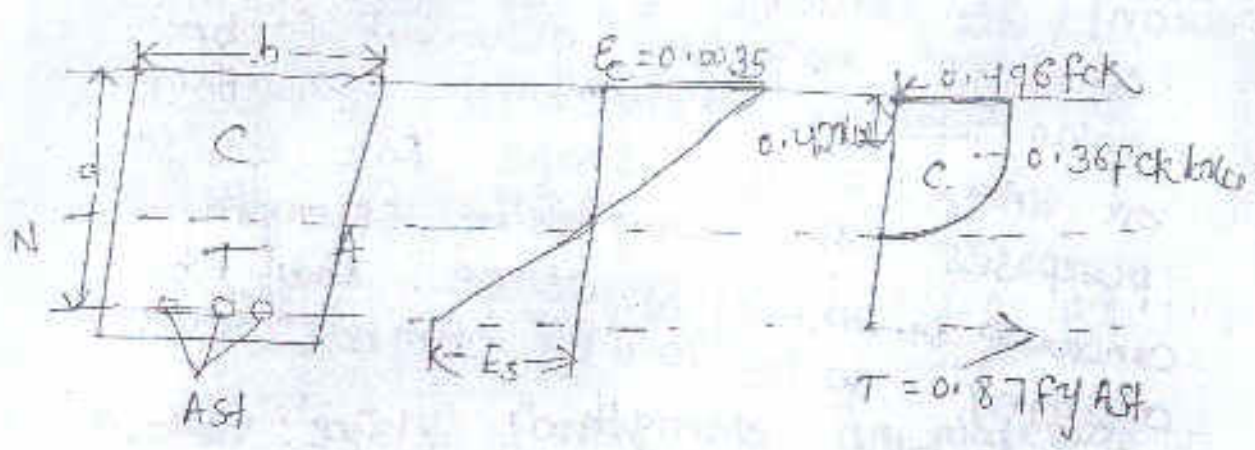
F_y = characteristic strength of steel

E_s = Young's modulus of steel

$$E = 2 \times 10^5 \text{ N/mm}^2$$

1 June 2021

Derivation formula for balanced singly reinforced rectangular beam :-



To find x_u

Total Compression = total tension

$$0.36 f_{ck} b x_u = 0.87 f_y A_{st}$$

$$x_u = \frac{0.87 f_y A_{st}}{0.36 f_{ck} b}$$

To find Lever Arm (z)

$$z = d - 0.42 x_u$$

To find out Moment of Resistance

$$M_R = \text{total compression} \times LA$$

(or)

$$\text{total tension} \times LA$$

$$M_R = 0.36 f_{ck} b x_u \left(d - 0.42 x_u \right)$$

$$= \frac{0.36 f_{ck} b x_u}{d} \left(\frac{d}{d} - \frac{0.42 x_u}{d} \right)$$

$$\Rightarrow 0.36 f_{ck} \frac{x_u}{d} (1 - 0.42 \frac{x_u}{d}) b$$

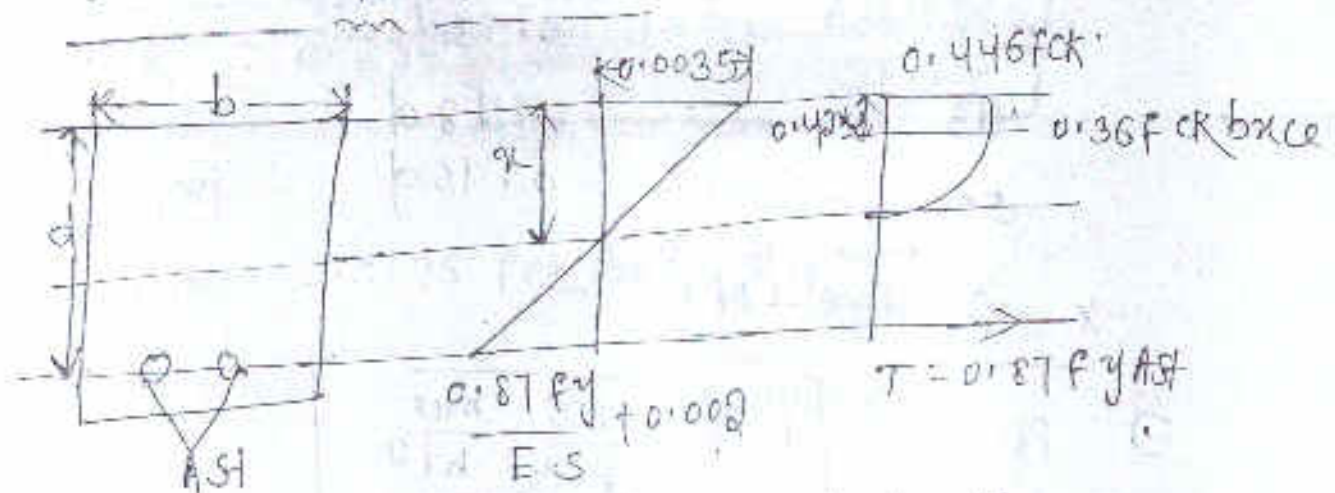
(*)

$$M_R = 0.87 f_y A_{st} (d - 0.42 x_u)$$

$$= 0.87 f_y A_{st} \left(d - 0.42 \left(\frac{0.87 f_y A_{st}}{0.36 f_{ck} b} \right) \right)$$

$$= 0.87 f_y A_{st} d \left(1 - \frac{f_y A_{st}}{f_{ck} b d} \right)$$

Maximum depth of N.A



By the geometry of the strain dia

$$\frac{x_{u \max}}{d} = \frac{0.0035}{\frac{0.87 f_y}{E_s} + 0.002 + 0.0035}$$

$$\frac{x_{u \max}}{d} = \frac{0.0035}{\frac{0.87 f_y}{2 \times 10^5} + 0.002 + 0.0035}$$

$$\frac{x_{u,max}}{d} = \frac{750}{1100 + 0.87 f_y}$$

2 June 2021

f_y (N/mm ²)	$\frac{x_{u,max}}{d}$
250	0.53
415	0.48
500	0.46

$$\frac{x_{u,max}}{d} = 0.53$$

$$x_{u,max} = 0.53d$$

f_y (N/mm ²)	$x_{u,max}$
250	0.53d
415	0.48d
500	0.46d

% of steel (Pt)

$$P_t = 50 \left[\frac{1 - \sqrt{1 - \frac{4.6}{f_{ck}} \frac{m_u}{bd^2}}}{f_y / f_{ck}} \right]$$

$$P_{t,limit} = 50 \left[\frac{1 - \frac{4.6}{f_{ck}} \frac{m_{u,limit}}{bd^2}}{f_y / f_{ck}} \right]$$

If $x_u < x_{u,max}$, the section is under reinforced section

$$M_R = 0.87 f_y A_s t d \left[1 - \frac{A_s t f_y}{bd f_{ck}} \right]$$

If $x_u > x_{u, \max}$, the beam is over reinforced section.

$$M_{R, \text{limit}} = 0.36 f_{ck} b x_u \left(d - 0.42 \frac{x_{u, \max}}{d} \right)^2$$

$$M_R = 0.36 f_{ck} b x_u \left(d - 0.42 x_u \right)$$

Grade of steel $\frac{x_{u, \max}}{d}$ $M_{u, \text{limit}}$

Fe 250 $\frac{0.53}{0.53}$ $0.148 f_{ck} b d^2$

Fe 415 $\frac{0.48}{0.48}$ $0.138 f_{ck} b d^2$

Fe 500 $\frac{0.46}{0.46}$ $0.133 f_{ck} b d^2$

For balanced section

$$M_R = 0.87 f_{yk} A_{st} d \left[1 - \frac{A_{st} f_{yk}}{b d f_{ck}} \right]$$

(iii)

$$M_{u, \text{limit}} = 0.36 f_{ck} b d^2 \cdot \frac{x_{u, \max}}{d} \times \left(1 - 0.42 \frac{x_{u, \max}}{d} \right)$$

18 A rectangular reinforced conc. beam has a width of 200mm & effective depth 460mm is reinforced with 2 bars of 20mm dia bar. The materials are M20 grade concrete & Fe415 grade of steel. Calculate the ultimate moment of resistance of the section.

Given data

$$\text{Width of beam (b)} = 200 \text{ mm}$$

$$\text{Effective depth} = 460 \text{ mm}$$

$$A_{st} = 2 \times \frac{\pi}{4} \times 20^2 = 628.318 \text{ mm}^2$$

$$\text{For M20 grade conc. } f_{ck} = 20 \text{ N/mm}^2$$

$$\text{Fe415 Steel } f_y = 415 \text{ N/mm}^2$$

Step 1

Depth of NA (x_u)

$$x_u = \frac{0.87 f_y A_{st}}{0.36 f_{ck} b}$$

$$= \frac{0.87 \times 415 \times 628}{0.36 \times 20 \times 200}$$

$$= 357.45 \text{ mm}$$

$$= 357.45 \text{ mm}$$

$$= 357.45 \text{ mm}$$

Max^m depth of N.A ($x_{u \text{ max}}$)

$$x_{u \text{ max}} = 0.48 d$$

$$= 0.48 \times 460 = 220.8 \text{ mm}$$

$x_u < x_{u \text{ max}}$ so under reinforced section.

Step 2

ultimate moment of resistance

$$M_u = 0.87 f_y A_{st} d \left[1 - \frac{A_{st} f_y}{b d f_{ck}} \right]$$

$$= 0.87 \times 415 \times 628 \times 460$$

$$\left[1 - \frac{628 \times 415}{200 \times 460 \times 20} \right]$$

$$= 89526918.39 \text{ Nmm}$$

$$= 89.52 \text{ kNm}$$

Q2 A singly reinforced rectangular beam of width 230mm & 460mm effective depth is reinforced with 5 nos of 20mm dia bars. The materials are M20 grade Fe 415. Calculate ultimate moment of Resistance of section.

3 June 2021

soln

Given data :-

width of beam (b) = 230mm

Effective depth (d) = 460mm

$$A_{st} = 5 \times \frac{\pi}{4} \times 20^2 = 1570.79 \text{ mm}^2$$

for M20 grade $f_{ck} = 20 \text{ N/mm}^2$

Fe 415 $f_y = 415 \text{ N/mm}^2$

Step 1

depth of N.A x_u

$$x_u = \frac{0.87 \times 415 \times 1570}{0.36 \times 20 \times 230} = 342.29 \text{ mm}$$

max^m depth of N.A ($x_{u,max}$)

$$\frac{x_{u,max}}{d} = 0.48 \Rightarrow x_{u,max} = 0.48 \times 460 = 220.8 \text{ mm}$$

Step - $x_u > x_{u,max}$ So the beam is over reinforced section.

$$M_R = 0.138 f_{ck} b d^2$$

$$= 0.138 \times 20 \times 230 \times 460^2$$

$$= 134323680 \text{ Nmm}$$

$$= 134.32 \text{ kNm}$$

Q3 A reinforced concrete beam 300mm width is reinforced with 1436 mm^2 of Fe415 HYSD bars at an effective depth of 500mm. If M20 grade concrete is used estimate the moment of resistance of the section by LSM.

Solⁿ width of beam (b) = 300mm

Effective depth = ~~435 mm~~ 500mm

$A_{st} = 1436 \text{ mm}^2$

M20 grade (f_{ck}) = 20 N/mm^2

Fe415 = 415 N/mm^2

Step-1

$$x_{ie} = \frac{0.87 \times 415 \times 1436}{0.36 \times 20 \times 300}$$

$$= 240.03 \text{ mm}$$

max^m depth of n.A. $x_{u,max}$

$$0.48 \times 500 = 240 \text{ mm}$$

$x_u = x_{u,max}$

section.

So the beam is balanced

$$\begin{aligned}
 MR &= 0.138 f_{ck} b d^2 = 0.138 \times 20 \times 300 \times 500^2 \\
 &= 2070000 \text{ Nm} \\
 &= 207 \text{ kNm}
 \end{aligned}$$

To find out steel area for a given factored moment :-

Step-1

For a given factored moment

(1.5x working moment) & assumed width of the section.

Step-2

Find out depth (if depth not given)

$$d = \sqrt{\frac{M_{u \text{ limit}}}{f_{ck} \times b \times \text{constant}}}$$

$$M_{u \text{ limit}} = 0.148 f_{ck} b d^2$$

$$= 0.138 f_{ck} b d^2$$

$$= 0.133 f_{ck} b d^2$$

If depth given: —

calculate $M_{u \text{ limit}}$ value according to this value. Compare with ' M_u '

Choose the section.

If $M_{u \text{ limit}} > M_u$ it is under reinforced section.

$$M_u = 0.87 A_{st} F_y d \left[1 - \frac{F_y A_{st}}{f_{ck} b d} \right]$$

(iii) If $M_{u\max} = M_u$, then it is balance section.

$$\frac{M_{u\max}}{d} = \frac{0.87 F_y A_{st}}{0.36 f_{ck} b d}$$

30 Determine the area of reinforcement required for a singly reinforced conc. section having a width of 300 mm and an effective depth of 600 mm to resist a factored moment of 200 kNm. The materials are M20 grade conc. & HYSD reinforcement of grade Fe415.

data given

width of (b) = 300 mm

Effective depth (d) = 600 mm

factored moment (M_u) = 200 kNm
= 200×10^6 Nmm

M20 grade (f_{ck}) = 20 N/mm²

HYSD Fe415 (F_y) = 415 N/mm²

Step-1

$$\begin{aligned} M_{u\text{limit}} &= 0.138 f_{ck} b d^2 \\ &= 0.138 \times 20 \times 300 \times 600^2 \\ &= 298,080,000 \text{ Nmm} \\ &= 298 \text{ kNm} \end{aligned}$$

$$M_{u \text{ limit}} = 298 \text{ kNm}$$

$$M_u = 200 \text{ kNm}$$

$M_{u \text{ limit}} > M_u$ so it is under reinforced section.

Step 2
find steel area

$$M_u = 0.87 A_{st} f_y d \left[1 - \frac{f_y A_{st}}{f_{ck} b d} \right]$$

$$200 \times 10^6 = 0.87 \times A_{st} \times 415 \times 600 \left[1 - \frac{A_{st} \times 415}{20 \times 300 \times 600} \right]$$

$$\Rightarrow 200 \times 10^6 = 216630 A_{st} \left(1 - 1.15 \times 10^{-4} A_{st} \right)$$

$$\Rightarrow 200 \times 10^6 = 216630 A_{st} - 24.91 A_{st}^2$$

4 June 2021

26

Determine the area of reinforcement required for a singly reinforced concrete section having a width of 230 mm resist a factored moment of 300 kNm. The materials are M20, grade conc. & HYSD reinforcement of grade Fe 415.

Solⁿ Given data:—

$$\text{width of beam } (b) = 230 \text{ mm}$$

$$\text{Factored moment} = 300 \text{ kNm}$$

$$f_{ck} = 20 \text{ N/mm}^2$$

$$f_y = 415 \text{ N/mm}^2$$

Step-1

Find effective depth of beam (d).

$$d = \sqrt{\frac{m_{ulimit}}{f_{ck} \times b \times \text{constant}}}$$

$$m_{ulimit} = 0.138 f_{ck} b d^2$$

$$d = \sqrt{\frac{300 \times 10^6}{20 \times 230 \times 0.138}} = 687.45 \approx 688 \text{ mm}$$

Step-2

$$M_{ulimit} = 0.138 f_{ck} b d^2$$

$$= 0.138 \times 20 \times 230 \times 688^2$$

$$= 300 \text{ kNm}$$

$$M_u = 300 \text{ kNm}$$

$$M_{u \text{ limit}} = 300 \text{ kNm}$$

$M_u = M_{u \text{ limit}}$ it is balanced section.

Step-3

Area of steel

$$\frac{m_{u \text{ max}}}{d} = \frac{0.87 f_y A_{st}}{0.36 f_{ck} b d}$$

$$0.48 = \frac{0.87 \times 415 A_{st}}{0.36 \times 200 \times 230 \times 688}$$

$$546877.44 = 0.87 \times 415 A_{st}$$

$$A_{st} = \frac{546877.44}{0.87 \times 415} = 1514 \text{ mm}^2$$

Q. A singly reinforced beam is subjected to a bending moment of 36 kNm at working loads. The width of beam is 200 mm. Find the depth & steel area of the section. The materials are M20 grade concrete & HYSD reinforcement.

Given data:-

bending moment = 36 kNm at working loads

factored moment = (1.5 × working loads)

$$(1.5 \times 36) = 54 \text{ kNm}$$

width of beam (b) = 200mm

M20 grade $f_{ck} = 20 \text{ N/mm}^2$

HYSD Fe415 $F_y = 415 \text{ N/mm}^2$

Step-1

$$d = \sqrt{\frac{M_u}{f_{ck} \times b \times \text{Constant}}}$$
$$= \sqrt{\frac{54 \times 10^6}{20 \times 200 \times 0.138}}$$
$$= 312.77 \approx 313 \text{ mm}$$

$$M_{u \text{ limit}} = 0.138 \times 20 \times 200 \times 313^2$$

$$= 53733888 \text{ Nmm}$$

$$= 53707888 \text{ Nmm} = 54 \text{ kNm}$$

$$M_u = 54 \text{ kNm}$$

$$M_{u \text{ limit}} = 54 \text{ kNm}$$

then the beam is balanced section.

Step-2

Area of steel

$$\frac{m_{\text{max}}}{d} = \frac{0.87 F_y A_{st}}{0.36 f_{ck} b d}$$

$$0.48 = \frac{0.87 \times 415 A_{st}}{0.36 \times 20 \times 200 \times 313}$$

$$\frac{216345.6}{0.87 \times 415} = 481$$

$$A_{st} = 599.21 \text{ mm}^2$$

$$216.34575 = 0.87 \times 415 A_{st}$$

$$A_{st} = \frac{216.34575}{0.87 \times 415}$$

$$0.48 = \frac{0.87 \times 415 \times A_{st}}{0.38720 \times 2.30 \times 688}$$

$$54.6877 = 44 = A_{st}$$

$$0.87 \times 415$$

$$\Rightarrow 1514 \text{ mm}^2 = A_{st}$$

Q A singly reinforced concrete beam subjected to a bending moment 56 kNm at working loads. The width of beam is 230 mm. balanced design. Find depth & steel area. The materials are M20 grade conc. & HY 50 reinforcement.

Given data -

$$\text{Moment} = 56 \text{ kNm}$$

$$M_u = 1.5 \times 56 = 84 \text{ kNm}$$

$$\text{width of beam (b)} = 230 \text{ mm}$$

$$\text{M20 grade } f_{ck} = 20 \text{ N/mm}^2$$

$$(f_y = 415 \text{ N/mm}^2)$$

$$d = \sqrt{\frac{84 \times 10^6}{20 \times 230 \times 0.138}}$$

$$= 363.76 \text{ mm}$$

Step - 2

Area of steel

numer

0.87 F_y A_{st}

d

0.36 F_{ck} b d

$$0.48 = \frac{0.87 \times 415 A_{st}}{0.36 \times 20 \times 230 \times 354}$$

$$A_{st} = \frac{216345.6}{0.87 \times 415}$$

$$\Rightarrow \frac{289336.32}{0.87 \times 415} = A_{st}$$

$$\Rightarrow A_{st} = \frac{289336.32}{0.87 \times 415} = 801.37 \text{ mm}^2$$

Q30 A rectangular beam 230 mm wide and 250 mm effective depth is reinforced with 4 no 16 mm diameter bars. Find out the depth of neutral axis and specify the type of beam. The materials are 120 grade conc. and HYSD reinforcement of grade Fe415. Also find out the depth of neutral axis if the reinforcement is increased to 4 no. 20 mm diameter bars.

Given data :-

width of beam (b) = 230 mm

Effective depth (d) = 250 mm

no of bars = 4

dia = 16 mm

A_{st} = 804 mm²

Case-1

$$A_{st} = 3 \times \frac{\pi}{4} \times 20^2 = 942.47 \text{ mm}^2$$

Step 1

$$\mu_w = \frac{0.87 \times f_y \times A_{st}}{0.36 \times 20 \times 230} = \frac{0.87 \times 415 \times 942.47}{0.36 \times 20 \times 230}$$
$$= 205.48$$

Step-2

$$\mu_{max} = 0.48 \times 460 = 220.8$$

$\mu_w < \mu_{max}$
and is reinforced

So the beam is
section.

Step-3

$$M_u = 0.87 f_y A_{st} d \left[1 - \frac{A_{st} f_y}{b d f_{ck}} \right]$$
$$= 0.87 \times 415 \times 942.47 \times 460 \left[1 - \frac{942.47 \times 415}{230 \times 460 \times 20} \right]$$
$$= 126672921.5 \text{ N}\cdot\text{mm}$$
$$= 126.67 \text{ kNm}$$

Case-2 $A_{st} = 5 \times \frac{\pi}{4} \times 20^2 = 1570.79 \text{ mm}^2$

Step-1

$$\mu_w = \frac{0.87 f_y A_{st}}{0.36 \times 20 \times 230} = 342.47$$

Step-2

$$\mu_{max} = 0.48 \times 460 = 220.8$$

Step-1

$$x_u = \frac{0.87 F_y A_{st}}{0.36 f_{ck} b} = \frac{0.87 \times 415 \times 804}{0.36 \times 20 \times 230} = 175.29 \text{ mm}$$

Step-2 max^m depth of N.A (x_{u,max})

$$0.48d = 0.48 \times 520 = 249.6 \text{ mm}$$

$x_u < x_{u,max}$ so the beam is in under reinforced section.

Case 2

$$A_{st} = 4 \times \frac{\pi}{4} \times 20^2 = 1256.63 \text{ mm}^2$$

Step N.A (x_u) depth of

$$x_u = \frac{0.87 \times 415 \times 1256.63}{0.36 \times 20 \times 230} = 273.97 \text{ mm}$$

60 A singly reinforced rectangular beam of width 230 mm and 460 mm effective depth is reinforced with 3 no 20 mm diameter bars. find out the factored moment of resistance of the section. The materials are M20 grade concrete and HYSD reinforcement of grade Fe 415. Also find out the factored moment of resistance if it is reinforced with 9 no 20 mm dia.

61

Given data:-

width of beam (b) = 230 mm

Effective depth (d) = 460 mm

$f_{ck} = 20 \text{ N/mm}^2$

$f_y = 415 \text{ N/mm}^2$

is max & is
over reinforced

so the beam is
section.

Step-3

$$M_{lim} = 0.138 \times f_{ck} b d^2$$

$$= 0.138 \times 20 \times 230 \times 160^2$$

$$= 134323680 \text{ Nmm}$$

$$= 134.32 \text{ kNm}$$

Q1 A rectangular cantilever beam of size 230 mm width \times 500 mm effective depth is subjected to a bending moment of 80 kNm at working loads. Find the steel area required. The materials are M20 grade concrete and reinforcement of grade Fe415.

Sol

Given data :-

Width of beam (b) = 230 mm

Effective depth (d) = 500 mm

bending moment = 80 kNm

Factor moment = $1.5 \times 80 = 120 \text{ kNm}$

$f_{ck} = 20 \text{ N/mm}^2$

$$f_{y} = 415 \text{ N/mm}^2$$

Step-1

$$M_{u \text{ limit}} = 0.138 f_{ck} b d^2$$

$$= 0.138 \times 20 \times 230 \times 500^2$$

$$= 158.70 \text{ kNm}$$

$M_u < M_{u \text{ limit}}$, so the beam under reinforced section.

$$M_u = 0.87 A_{st} f_y d \left[1 - \frac{f_y A_{st}}{f_{ck} b d} \right]$$

$$= 120 \times 10^6 = 0.87 \times A_{st} \times 415 \times 500$$

$$\left[1 - \frac{415 \times A_{st}}{20 \times 230 \times 500} \right]$$

$$\Rightarrow 120 \times 10^6 = 180525 A_{st} (1 - 1.80 \times 10^{-4} A_{st})$$

$$\Rightarrow 120 \times 10^6 = 180525 A_{st} - 32.49 A_{st}^2$$

$$\Rightarrow 32.49 A_{st}^2 - 180525 A_{st} + 120 \times 10^6 = 0$$

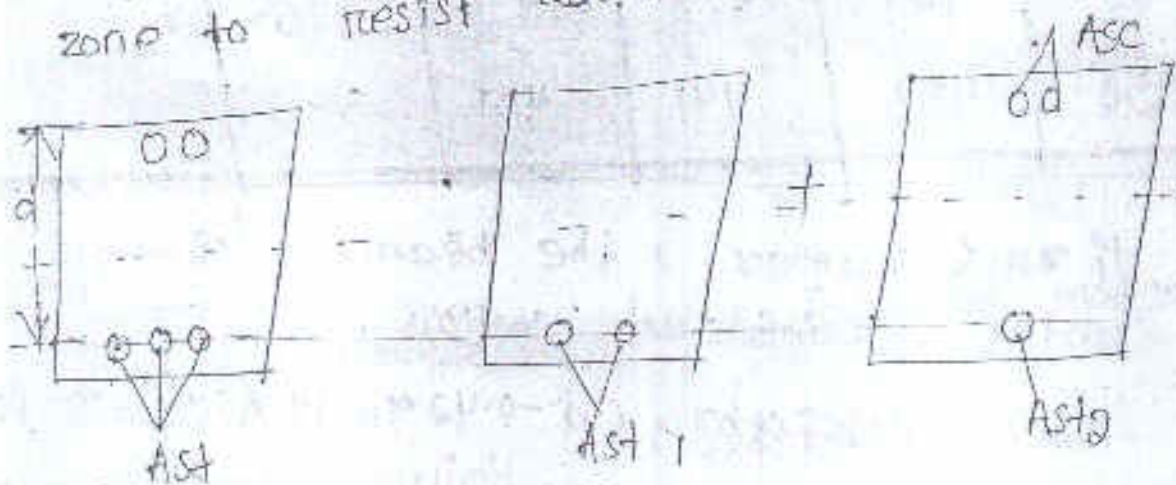
$$\Rightarrow A_{st} = 4784.33 \text{ mm}^2$$

7 June 2021

Doubly reinforced Beam

For design moment M_u if the size of the rectangular beam section is fixed and limiting moment of resistance of singly reinforced section is less than M_u . There are two methods to design such beam :-

- ① Increase the ~~size~~ conc. mix to increase the capacity of section?
- ② Reinforcement are provided in compression zone to resist additional moment.



$$M_{uc} = M_{ulimit} + M_2$$

$$A_{st} = A_{s1} + A_{s2}$$

$$A_{s2} = \frac{A_{sc} \times f_{sc}}{0.87 f_y}$$

$$A_{s1\text{ limit}} = \frac{M_{ulimit}}{0.87 f_y (d - 0.42 x_{u\text{max}})}$$

$$A_{sc} = \frac{M_{u2}}{f_{sc} (d - d')}$$

To find out depth of n.a

$$0.36 f_{ck} b x_u + f_{sc} A_{sc} = 0.87 f_y A_{st}$$

stress in compression zone

F _y N/mm ²	d'/d			
	0.05	0.1	0.15	0.2
250	217	217	217	217
415	355	353	342	329
500	424	412	395	370
550	458	441	419	380

If $x_u < x_{u,max}$, the beam is in under reinforced section.

$$M_u = 0.36 f_{ck} b x_u (d - 0.42 x_u) + A_{sc} (f_{sc} - f_{sc}) (d - d')$$

$$M_u = 0.36 f_{ck} b x_u (d - 0.42 x_u) + A_{sc} f_{sc} (d - d')$$

If $x_u > x_{u,max}$ over reinforced beam.

$$M_u = M_{u,limit} + f_{sc} A_{sc} (d - d')$$

(over & balanced)

Types of problems

Type-1

To find out the moment of resistance of the given section.

$$c = T$$

$$0.36 f_{ck} b x_{uT} A_{sc} (f_{sc} - f_{cc}) = 0.87 f_y A_{st}$$

$$x_{u,max} = ?$$

If $x_u < x_{u,max}$ the beam is under reinforced section

If $x_u > x_{u,max}$ the beam is over reinforced section

Type-2

Find out reinforcement & factored moment:—

① Find out $M_{u,limit} = 0.148 f_{ck} b d^2$

for 415 = $0.138 f_{ck} b d^2$

for 500 = $0.133 f_{ck} b d^2$

$$A_{st,limit} = \frac{M_{u,limit}}{0.87 f_y (d - 0.42 x_{u,max})}$$

② $M_{u2} = M_u - M_{u,limit}$

③ Find compression zone steel area

$$A_{sc} = \frac{M_{u2}}{f_{sc} (d - d')}$$

step-4

Area of steel in tension

$$A_{stg} = A_{sc} f_{sc}$$

$$0.87 f_y$$

$$A_{st} = A_{s,lim} + A_{stg}$$

8 June 2021

18 A doubly reinforced beam section is 250 mm wide & 450 mm deep to the centre of the tensile reinforcement. It is reinforced with 2 bars of 16 mm dia. AS compression reinforcement at an effective cover of 50 mm & 4 bars of 25 mm dia bar as tensile steel. Calculate the ultimate moment of resistance. Use M20 grade conc. & HYSD reinforcement.

Given data:-

$$\text{Width of beam } (b) = 250 \text{ mm}$$

$$\text{Effective depth } (d) = 450 \text{ mm}$$

$$A_{sc} = 2 \times \frac{\pi}{4} \times 16^2 = 402 \text{ mm}^2$$

$$A_{st} = 4 \times \frac{\pi}{4} \times 25^2 = 1963.49 \approx 1964 \text{ mm}^2$$

$$f_{ck} = 20 \text{ N/mm}^2$$

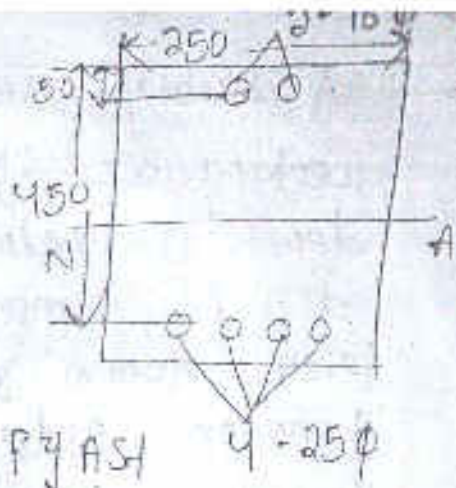
$$f_y = 415 \text{ N/mm}^2$$

$$\frac{d'}{d} = \frac{50}{450} = 0.11$$

$$f_{sc} = 353 \text{ N/mm}^2$$

Step 1

To find depth of n.A



$$C = T$$

$$0.36 f_{ck} b x_u + f_{sc} A_{sc} = 0.87 f_y A_{st}$$

$$\Rightarrow 0.36 \times 20 \times 250 x_u + 353 \times 400 = 0.87 \times 415 \times 1964$$

$$\Rightarrow 1800 x_u + 141900 = 709102.2$$

$$\Rightarrow x_{u_{max}} = \frac{709102.2 - 141900}{1800}$$

$$\Rightarrow x_u = \frac{709102.2 - 141900}{1800} = 315 \text{ mm}$$

$$x_{u_{max}} = 0.48 d$$

$$= 0.48 \times 450 = 216 \text{ mm}$$

$x_u > x_{u_{max}}$ the beam is in over reinforced section.

Step-2

To find ultimate moment of resistance (M_u)

$$M_u = M_{u_{lim}} + f_{sc} A_{sc} (d - d')$$

$$M_{u_{lim}} = 0.138 \times 20 \times 250 \times 400^2$$

$$= 139.72 \text{ kNm}$$

$$M_u = 139.72 \times 10^6 + 353 \times 400 \times (450 - 50)$$

$$= 196.48 \text{ kNm}$$

2.8

A doubly reinforced conc. beam having rectangular section 250×540 mm overall depth is reinforced with 2 bars of 12 mm dia in compression side of effective cover 40 mm & 4 bars 20 mm dia in tension side. Use M20 conc. & Fe415 steel. Calculate flexural strength of the section. Take effective depth cover 40 mm both side.

Given data:-

$$\text{Width of beam} = 250 \text{ mm}$$

$$\text{Overall depth (D)} = 540 \text{ mm}$$

$$\text{Effective cover (d')} = 40 \text{ mm}$$

$$d = 540 - 40 = 500 \text{ mm}$$

$$\frac{d'}{d} = \frac{40}{500} = 0.08 \quad f_{sc} = 353 \text{ N/mm}^2$$

$$A_{st} = 1256 \text{ mm}^2$$

$$\text{M20 grade } f_{ck} = 20 \text{ N/mm}^2$$

$$A_{sc} = 226 \text{ mm}^2$$

$$\text{Fe415 (Fy)} = 415 \text{ N/mm}^2$$

Step-1

$$m_{\text{limit}} = 0.138 f_{ck} b d^2$$

$$= 0.138 \times 20 \times 250 \times 500^2$$

$$= 170.5 \text{ kNm}$$

$$x_{u \text{ max}} = 0.48 d = 0.48 \times 500$$

$$= 240 \text{ mm}$$

$$A_{st1} \text{ limit} = \frac{\text{Mie limit}}{0.87 f_y (\rho - 0.42 \rho_{\text{lim}})}$$

$$= \frac{172.7 \times 10^6}{0.87 \times 415 (500 - 0.42 \times 514)}$$

$$= 1196.8 \approx 1197 \text{ mm}^2$$

$$A_{st} = 1256 \text{ mm}^2$$

$$A_{st2} = \frac{f_{sc} \times A_{sc}}{0.87 f_y} = \frac{353 \times 226}{0.87 \times 415}$$

$$= 226.96 \approx 227 \text{ mm}^2$$

$$A_{st} = A_{st1} + A_{st2}$$

$$A_{st1} = A_{st} - A_{st2}$$

$$= 1256 - 227 = 1035 \text{ mm}^2$$

Step 2

To find ρ_w

$$0.36 f_{ck} b d + f_{sc} A_{sc} = 0.87 f_y A_{st}$$

$$\rho_w = \frac{0.87 f_y A_{st}}{0.36 f_{ck} b + f_{sc} A_{sc}}$$

$$= \frac{0.87 \times 415 \times 1256}{0.36 \times 20 \times 250 + 353 \times 226} = \frac{0.87 \times 415 \times 1256}{1800 + 79778}$$

$$= \frac{453478.8}{81778} = 5.5478$$

$$\rho_w = \frac{453478.8}{81778} = 5.5478$$

$$\rho_w = \frac{453478.8}{81778} = 5.5478$$

$\rho_w =$

0.0055

$$x_{u\max} = 240 \quad x = 267$$

$x_u < x_{u\max}$ so it is under reinforced section.

$$\begin{aligned} M_u &= 0.36 f_{ck} b x_u (d - 0.42 x_u) + A_s c f_{sc} (d - d') \\ &= 0.36 \times 20 \times 250 \times 267 \cdot 81 (500 - 0.42 \times 267 \cdot 81) \\ &\quad + 226 \times 353 (500 - 40) \\ &= 191079022.9 \text{ Nm} \\ &= 191 \text{ kNm} \end{aligned}$$

9 June 2021

3Q

A rectangular beam of size 230mm wide \times 500mm effective depth is subjected to a factored moment of 200 kNm. Find the reinforcement for flexure. The materials are M20 grade conc. & Fe415 steel. Take Cover = 50mm.

Solⁿ

Given data :-

$$\text{width of beam } (b) = 230 \text{ mm}$$

$$\text{Effective depth } (d) = 500 \text{ mm}$$

$$f_{ck} = 20 \text{ N/mm}^2$$

$$f_y = 415 \text{ N/mm}^2$$

$$\text{factored moment } (M_u) = 200 \text{ kNm}$$

$$M_{u \text{ limit}} = 6.138 \text{ kNm}$$

$$= 158.7 \text{ kNm}$$

$M_{u \text{ limit}} < M_u$ so the beam is design as doubly reinforcement.

Step-1

$$M_{u \text{ limit}} = 158.7 \text{ kNm}$$

$$M_u = 200 \text{ kNm}$$

$$M_{u2} = M_u - M_{u \text{ limit}}$$

$$= 200 - 158.7 = 41.3 \text{ kNm}$$

Assume $d' = 50 \text{ mm}$

$$\frac{d'}{d} = \frac{50}{500} = 0.1 \quad f_{sc} = 353 \text{ N/mm}^2$$

$$A_{sc} = \frac{M_{u2}}{f_{sc}(d-d')} = \frac{41.3 \times 10^6}{353(500-50)}$$

$$= 260 \text{ mm}^2$$

$$A_{st2} = \frac{A_{sc} f_{sc}}{0.87 f_y} = \frac{260 \times 353}{0.87 \times 415} = 254 \text{ mm}^2$$

$$k_{u \text{ max}} = 0.48 \times 500 = 240 \text{ mm}$$

$$A_{st \text{ limit}} = \frac{M_{u \text{ limit}}}{0.87 f_y (d - 0.42 k_{u \text{ max}})}$$

$$= \frac{158.7 \times 10^6}{0.87 \times 415 \times (500 - 0.42 \times 240)} = 1101.08 \text{ mm}^2$$

$$A_{st} = A_{st\text{limit}} + A_{st2} = 1355 + 0.8 \text{ mm}^2$$

$$A_{sc} = 260 \text{ mm}^2$$

provide 2 bars 16 mm dia $A_{sc} = 2 \times \frac{\pi}{4} \times 16^2$
 $= 402 \text{ mm}^2$

$A_{st} = 1355$ provide 5 no 20 mm dia bar

$$A_{st} = 5 \times \frac{\pi}{4} \times 20^2 = 1570 \text{ mm}^2$$

$$\mu_u = 0.36 f_{ck} b \mu + f_{sc} A_{sc} = 0.87 \times F_y \times A_{st}$$

$$\Rightarrow 0.36 \times 20 \times 230 \mu + 353 \times 402 = 0.87 \times 415 \times 1570$$

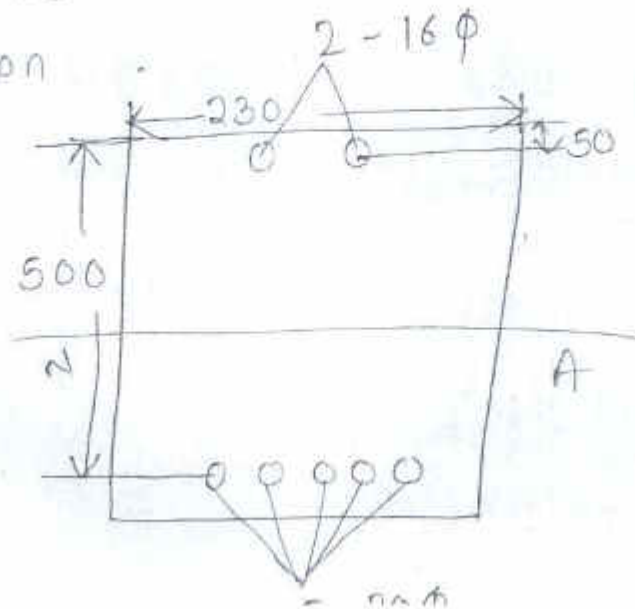
$$\Rightarrow 1656 \mu + 141906 = 566848.5$$

$$\Rightarrow 1656 \mu = 566848.5 - 141906$$

$$\Rightarrow \mu = \frac{566848.5 - 141906}{1656}$$

$$= 256 \text{ mm}^2$$

$\mu_u > \mu_{u\text{max}}$ the beam is over reinforced / section



10 June 2021

Q10 Find the factored moment of resistance of a beam section 300mm wide x 450mm effective depth reinforced with 2-20mm diameter bars as compression reinforcement at an effective cover of 50mm and 4-25mm diameter bars as tension reinforcement. The materials are M20 grade concrete and HYSD reinforcement of grade Fe415.

Given data:-

$$\text{Width of beam} = 300\text{mm}$$

$$\text{Effective depth} = 450\text{mm}$$

$$A_{sc} = 2 \times \frac{\pi}{4} \times 20^2$$
$$= 628 \text{ mm}^2$$

$$A_{st} = 4 \times \frac{\pi}{4} \times 25^2 = 1963 \text{ mm}^2$$

$$d' = 50\text{mm}$$

$$f_{ck} = 20 \text{ N/mm}^2$$

$$f_y = 415 \text{ N/mm}^2$$

$$f_{sc} = \frac{d'}{d} = \frac{50}{450} = 0.11 = 353 \text{ N/mm}^2$$

Step-1 $M_{ulimit} = 0.138 f_{ck} b d^2$

$$= 0.138 \times 20 \times 300 \times 450^2 = 167.67 \text{ kN}\cdot\text{m}$$

$$A_{st2} = \frac{A_{sc} f_{sc}}{0.87 f_y} = \frac{628 \times 353}{0.87 \times 415} = 613.9 \approx 614 \text{ mm}^2$$

$$A_{st\text{limit}} = A_{st} - A_{st2}$$

$$= 1963 - 614$$

$$= 1349$$

$$A_{st} = 614 + 1349 = 1963 \text{ mm}^2$$

Step 2

$$\frac{x_u}{d} \cdot 0.36 f_{ck} b x_u + f_{sc} A_{sc} = 0.87 f_y A_{st}$$

$$\Rightarrow 0.36 \times 20 \times 300 x_u + 353 \times 628 = 0.87 \times 415 \times 1963$$

$$\Rightarrow 2160 x_u + 221684 = 708741.15$$

$$\Rightarrow 2160 x_u = 708741.15 - 221684$$

$$\Rightarrow x_u = \frac{487057.15}{2160}$$

$$= 225.48$$

$$x_{u,max} = 0.48 x_d = 0.48 \times 450 = 216 \text{ mm}$$

$x_u > x_{u,max}$ so the beam is over reinforced/
section.

$$M_u = M_{u,limit} + f_{sc} A_{sc} (d - d')$$

$$= 1167.67 \times 10^6 + 353 \times 628 (450 - 50)$$

$$= 256343600 \text{ N}\cdot\text{mm}$$

$$= 256.34 \text{ kN}\cdot\text{m}$$

10 Jan 2021
Ex 50 Design a rectangular beam for an effective span of 6m. The super-imposed load is 80 kN/m and size of the beam is limited to 300mm x 700mm overall. Use M20 mix and Fe415 grade of steel.

Given data:-

Length of span = 6m

super-imposed load = 80 kN/m

$F_{ck} = 20 \text{ N/mm}^2$

$f_{yk} = 415 \text{ N/mm}^2$

width of beam 300mm = 300mm

overall depth = 700mm = 700mm

Dead load of beam = $b \times d \times 25$

$$= 0.3 \times 0.7 \times 25 = 5.25 \text{ kN/m}$$

total load of beam = self wt of beam + super-imposed load

$$= 5.25 + 80$$

$$\begin{aligned} \text{factor load} &= 85.25 \text{ kN/m} \\ \text{factorized moment} &= \left(1.5 \times \frac{85.25 \times 6^2}{8} \right) = \frac{128 \times 16^2}{8} \end{aligned}$$

$$= 576 \text{ kN.m}$$

Let effective cover = 40mm

Effective depth = $700 - 40 = 660 \text{ mm}$

$$f_{sc} = \frac{d'}{d} = \frac{40}{660} = 0.06 = 353 \text{ N/mm}^2$$

Step-1

Limiting moment

$$0.138 f_{ck} b d^2 = 0.138 \times 20 \times 300 \times 600^2$$

$$= 360676800 \text{ N}\cdot\text{mm}$$

$$= 360.67 \text{ kNm}$$

$M_u = 567 > M_{u\text{limit}} = 360$ so the design
doubly reinforced.

$$M_{u2} = M_u - M_{u\text{limit}}$$

$$= 567 - 360 = 216 \text{ kNm}$$

$$A_{sc} = \frac{M_{u2}}{f_{sc}(d-d')} = \frac{216 \times 10^6}{353 \times (660 - 40)}$$

$$= 986.93 \text{ mm}^2$$

$$A_{st2} = \frac{A_{sc} \times f_{sc}}{0.87 \times f_y} = \frac{986.93 \times 353}{0.87 \times 415}$$
$$= 964.42 = 965 \text{ mm}^2$$

$$\mu_{\text{max}} = 0.48 \times 660 = 316.8 \text{ mm} = 317 \text{ mm}$$

$$A_{st\text{limit}} = \frac{M_{u\text{limit}}}{0.87 f_y (d - 0.42 \mu_{\text{max}})}$$
$$= \frac{360.67 \times 10^6}{0.87 \times 415 (660 - 0.42 \times 317)}$$
$$= 1896 \text{ mm}^2$$

$$A_{st} = A_{st \text{ limit}} + A_{st2}$$

$$= 1986 + 965 = 2861 \text{ mm}^2$$

$$A_{sc} = 986.93 \text{ provide 4 bars } 20 \phi$$

$$A_{sc} = 4 \times \frac{\pi}{4} \times 20^2 = 1256 \text{ mm}^2$$

$$A_{st} = 2861 \text{ provide 6 bars } 25 \phi$$

$$A_{st} = 6 \times \frac{\pi}{4} \times 25^2 = 2945.24 \text{ mm}^2$$

Step-2

To find x_u

$$0.36 f_{ck} b x_u + f_{sc} A_{sc} = 0.87 f_y A_{st}$$

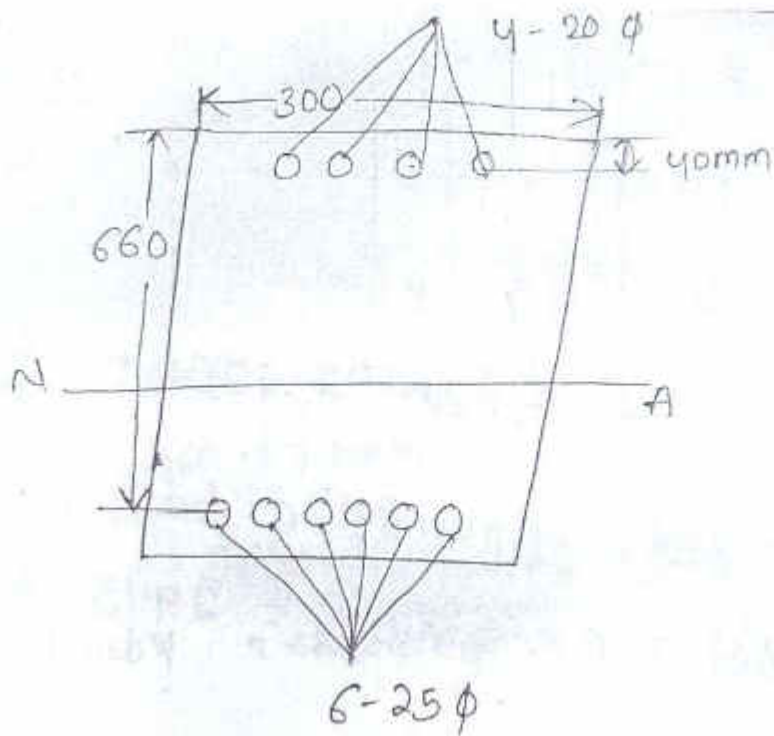
$$\Rightarrow 0.36 \times 20 \times 300 x_u + 353 \times 1256 \cdot 63 = 0.87 \times 415 \times 2945.24$$

$$\Rightarrow 2160 x_u + 443495.08 = 1063378.9$$

$$\Rightarrow 2160 x_u = 1063378.9 - 443495.08$$

$$\Rightarrow x_u = \frac{619883.82}{2160} = 286.9 \text{ mm}$$

$x_{u \text{ max}} > x_u$ the beam is under reinforced section.



11 June 2021

A doubly reinforced rectangular beam 300mm wide & 450mm effective depth having 3 no 12mm dia bars at compression side. at an effective cover of 40mm & 5 no of 20mm dia are tension side. Calculate factored moment & also specify type of beam. The materials are M20 grade concrete & mild steel reinforcement.

Given data:-

width of beam 300mm

Effective depth = 450mm

Effective cover = 40mm.

$$A_{sc} = 3 \times \frac{\pi}{4} \times 12^2 = 339.29 \text{ mm}^2$$

$$A_{st} = 5 \times \frac{\pi}{4} \times 20^2 = 1570.79 = 1571 \text{ mm}^2$$

M20 grade $f_{ck} = 20 \text{ N/mm}^2$

Fer 250 $f_{yk} = 250 \text{ N/mm}^2$

$$\frac{d'}{d} = \frac{40}{490} = 0.08 \approx 0.1$$

$$f_{sc} = 217 \text{ N/mm}^2$$

Step-1

To find out depth of n.a

$$0.36 f_{ck} b x_u + f_{sc} A_{sc} = 0.87 f_y A_{st}$$

$$\Rightarrow 0.36 \times 20 \times 300 x_u + 217 \times 339.29 = 0.87 \times 250 \times$$

$$\Rightarrow 2160 x_u + 73625.93 = 341692.5 \quad 1571$$

$$\Rightarrow 2160 x_u = 341692.5 - 73625.93$$

$$\Rightarrow x_u = \frac{268066.57}{2160} = 124.10 \text{ mm}$$

$$x_{u \max} = 0.53 d = 0.53 \times 450 = 238.5 \text{ mm}$$

$x_u < x_{u \max}$ so th beam is underreinforced section.

Step-2

$$M_u = 0.36 f_{ck} b x_u (d - 0.42 x_u) + A_{sc} f_{sc} (d - d')$$

$$= 0.36 \times 20 \times 300 \times 124.10 (450 - 0.42 \times 124.10) +$$

$$339.29 \times 217 (450 - 40)$$

$$= 136840216.5 \text{ Nm}$$

$$= 136.8 \text{ kNm}$$

$$\frac{d'}{d} = \frac{40}{450} = 0.08 \approx 0.1$$

$$f_{sc} = 217 \text{ N/mm}^2$$

Step-1

To find out depth of n.A

$$0.36 f_{ck} b x_u + f_{sc} A_{sc} = 0.87 f_y A_{st}$$

$$\Rightarrow 0.36 \times 20 \times 300 x_u + 217 \times 339.29 = 0.87 \times 250 \times 1571$$

$$\Rightarrow 2160 x_u + 73625.93 = 341692.5$$

$$\Rightarrow 2160 x_u = 341692.5 - 73625.93$$

$$\Rightarrow x_u = \frac{268066.57}{2160} = 124.10 \text{ mm}$$

$$x_{u \max} = 0.530 d = 0.53 \times 450 = 238.5 \text{ mm}$$

$x_u < x_{u \max}$ so th beam is underreinforced section.

Step-2

$$M_u = 0.36 f_{ck} b x_u (d - 0.42 x_u) + A_{sc} f_{sc} (d - d')$$

$$= 0.36 \times 20 \times 300 \times 124.10 (450 - 0.42 \times 124.10) +$$

$$339.29 \times 217 (450 - 40)$$

$$= 136840216.5 \text{ Nmm}$$

$$= 136.8 \text{ kNm}$$

$$= 268 \text{ kNm}$$

$x_u > x_{u\text{limit}}$ so the beam design as doubly reinforced beam.

$$\frac{d'}{d} = \frac{50}{500} = 0.1 \quad f_{sc} = 217 \text{ N/mm}^2$$

$$A_{st\text{limit}} = \frac{M_{u\text{limit}}}{0.87 f_y (d - 0.42 x_{u\text{max}})}$$

$$x_{u\text{max}} = 0.53 \times 550 = 291.5 \text{ mm}$$

$$A_{st\text{limi}} = \frac{268 \times 10^6}{0.87 \times 250 (550 - 0.42 \times 291.5)}$$
$$= 2881.82 \text{ mm}^2$$

$$M_u = M_{u\text{limit}} + M_{u2}$$

$$\Rightarrow M_{u2} = M_u - M_{u\text{limi}}$$
$$= 656 - 268 = 388 \text{ kNm}$$

$$A_{sc} = \frac{M_{u2}}{f_{sc} (d - d')} = \left(\frac{388 \times 10^6}{217 (550 - 50)} \right)$$
$$= 3576 \text{ mm}^2$$

$$A_{st2} = \frac{A_{sc} f_{sc}}{0.87 f_y} = \frac{3576 \times 217}{0.87 \times 250} = 3568 \text{ mm}^2$$

$$A_{st} = A_{st\text{lim}} + A_{st2} = 6449.82 \text{ mm}^2$$

$$A_{sc} = 3576 \text{ mm}^2 \quad \text{provide 6 bars } 30 \phi$$

$$A_{sc} = 6 \times \frac{\pi}{4} \times 30^2 = 4241.15 \text{ mm}^2$$

12 June 2021

0.5.14

Q Design rectangular beam for an effective span of 8m. The super-imposed load is 50 kN/m & size of the beam is 300mm x 550mm an effective depth use M20 grade concrete & Fe250 steel.

Soln

Given data :-

width of beam (b) = 300mm

Effective depth (d) = 550mm

d' = 50mm

super imposed load = 50 kN/m

span length = 8m

$f_{ck} = 20 \text{ N/mm}^2$

$f_{yk} = 250 \text{ N/mm}^2$

Soln

super imposed load = 50 kN/m

Self wt of beam = $b \times d' \times 25$

$$= 0.3 \times 0.6 \times 25 = 4.5 \text{ kN/m}$$

$D = 550 + 50 = 600 \text{ mm}$

total load = $50 + 4.5 = 54.5 \text{ kN/m}$

factored load = $1.5 \times 54.5 = 81.75 \text{ kN/m}$

$$= 82 \text{ kN/m}$$

factored moment = $\frac{wl^2}{8} = \frac{82 \times 8^2}{8}$

$$= 656 \text{ kNm}$$

Step 1

Multimit = $0.148 f_{ck} b d^2$

$$= 0.148 \times 20 \times 300 \times 550^2$$

$$= 268 \text{ kNm}$$

$x_u > x_{u\text{limit}}$ so the beam design as doubly reinforced beam.

$$\frac{d'}{d} = \frac{50}{500} = 0.1 \quad f_{sc} = 217 \text{ N/mm}^2$$

$$A_{st\text{limit}} = \frac{M_{u\text{limit}}}{0.87 f_y (d - 0.42 x_{u\text{max}})}$$

$$x_{u\text{max}} = 0.53 \times 550 = 291.5 \text{ mm}$$

$$A_{st\text{limi}} = \frac{268 \times 10^6}{0.87 \times 250 (550 - 0.42 \times 291.5)}$$
$$= 2881.82 \text{ mm}^2$$

$$M_{u2} = M_u - M_{u\text{limi}}$$

$$\Rightarrow M_{u2} = M_u - M_{u\text{limi}}$$
$$= 656 - 268 = 388 \text{ kNm}$$

$$A_{sc} = \frac{M_{u2}}{f_{sc} (d - d')} = \left(\frac{388 \times 10^6}{217 (550 - 50)} \right)$$
$$= 3576 \text{ mm}^2$$

$$A_{st2} = \frac{A_{sc} f_{sc}}{0.87 f_y} = \frac{3576 \times 217}{0.87 \times 250} = 3568 \text{ mm}^2$$

$$A_{st} = A_{st\text{lim}} + A_{st2} = 6449.82 \text{ mm}^2$$

$$A_{sc} = 3576 \text{ mm}^2 \quad \text{provide 6 bars } 30 \phi$$

$$A_{sc} = 6 \times \frac{\pi}{4} \times 30^2 = 4241.15 \text{ mm}^2$$

$$A_{st} = 6449.82 \text{ mm}^2$$

provide 7 bar 35ϕ

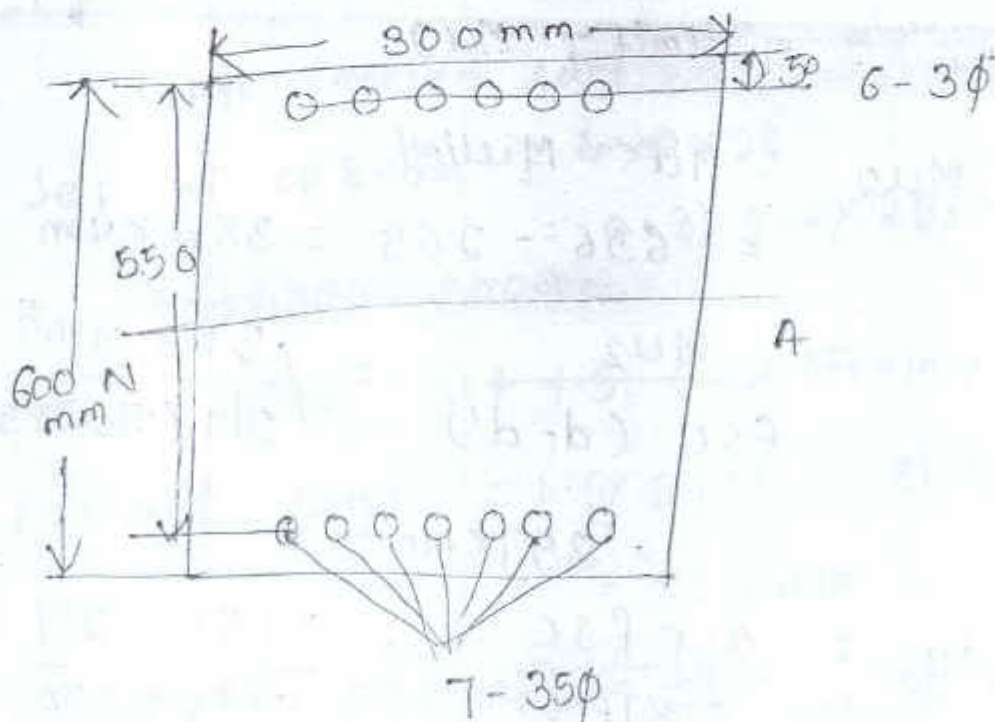
$$A_{st} = 7 \times \frac{\pi}{4} \times 35^2 = 6734.78 \text{ mm}^2$$

Step-2

$$\begin{aligned} 0.36 \times f_{ck} \times b \times u + f_{sc} \times A_{sc} &= 0.87 f_y A_{st} \\ 0.36 \times 20 \times 300 \times u + 217 \times 4241.15 &= 0.87 \times 250 \\ &\times 6734.78 \\ = 2160u + 920329.55 &= 1464814.65 \\ = 2160u &= \frac{544485.1}{2160} \end{aligned}$$

$$u = 252.07 \text{ mm}$$

So $u_{max} > u$ So the beam is under reinforced section.



$$A_{sc} = \frac{M_{u2}}{F_{sc}(d-d')} = \frac{181.4 \times 10^6}{217(550-50)}$$

$$= 1671.88 \text{ mm}^2$$

$$A_{stg} = \frac{A_{sc} \times F_{sc}}{0.87 \times f_y} = \frac{1671.88 \times 217}{0.87 \times 250}$$

$$= 1668.03 \text{ mm}^2$$

$$A_{st \text{ limit}} = \frac{M_{u \text{ limit}}}{0.87 f_y (d - 0.42 x_{u \text{ max}})}$$

$$x_{u \text{ max}} = 0.53 \times 550$$

$$= 291.5 \text{ mm}$$

$$= \frac{268.6 \times 10^6}{0.87 \times 250 \times (550 - 0.42 \times 291.5)}$$

=

$$= 2888.28 \text{ mm}^2$$

$$= 2888.28 \text{ mm}^2$$

$$A_{st} = A_{st \text{ limit}} + A_{stg}$$

$$= 2888.28 + 1668.03 = 4556.31 \text{ mm}^2$$

$$A_{sc} = 1671.88 \quad \text{provide 4 bar } 24 \text{ dia}$$

$$A_{sc} = 4 \times \frac{\pi}{4} \times 24^2 = 1809 \text{ mm}^2$$

$$A_{st} = 4556.31 \quad \text{provide 5 bar } 35 \text{ dia}$$

$$A_{st} = 5 \times \frac{\pi}{4} \times 35^2 = 4810.56 \text{ mm}^2$$

Step 2

To find μ_u

$$0.36 f_{ck} b x_u + f_{sc} A_{sc} = 0.87 f_y A_{st}$$

$$\Rightarrow 0.36 \times 20 \times 300 x_u + 217 \times 1809 = 0.87 \times 250 \times 4810.56$$

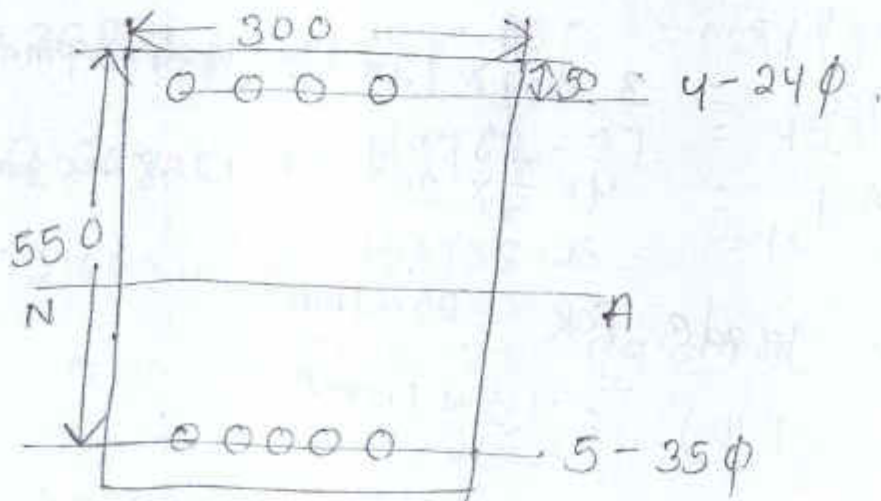
$$\Rightarrow 2160 x_u + 392553 = 1046296.8$$

$$\Rightarrow 2160 x_u = 1046296.8 - 392553$$

$$\Rightarrow x_u = \frac{653743.8}{2160} = 302 \text{ mm}$$

$$x_{u \max} = 291.5 \text{ mm}$$

$x_u > x_{u \max}$. the beam is over reinforced section.



19 Jun 2021

2/5

A doubly reinforced conc beam having rectangular section $300 \text{ mm} \times 540 \text{ mm}$ overall depth is reinforced with 3 bars of 12 mm dia. in compression side & 4 bars 20 mm dia at tension side. The effective cover to bars is 40 mm . use M20 grade concrete & HYSD reinforced. Calculate flexural strength of the section.

Solⁿ

$$\text{width of beam } (b) = 300 \text{ mm}$$

$$\text{overall depth } (D) = 540 \text{ mm}$$

$$\text{Effective cover } (d') = 40 \text{ mm}$$

$$\begin{aligned} \text{Effective depth } (d) &= D - d' = 540 - 40 \\ &= 500 \text{ mm} \end{aligned}$$

$$A_{sc} = 3 \times \frac{\pi}{4} \times 12^2 = 339.29 \text{ mm}^2$$

$$A_{st} = 4 \times \frac{\pi}{4} \times 20^2 = 1256.63 \text{ mm}^2$$

$$\text{M20 grade } f_{ck} = 20 \text{ N/mm}^2$$

$$(f_y) = 415 \text{ N/mm}^2$$

$$\frac{d'}{d} = \frac{40}{500} = 0.08 = 0.1$$

$$f_{sc} = 353 \text{ N/mm}^2$$

Step-1

$$A_{st2} = \frac{F_{sc} A_{sc}}{0.87 F_y} = \frac{353 \times 339.29}{0.87 \times 415} = 332 \text{ mm}^2$$

$$A_{st1} = A_{st} - A_{st2} = 1256.63 - 332 = 924.63 \text{ mm}^2$$

Step-2

$$M_{u \text{ limit}} = 0.138 F_{ck} b d^2$$

$$= 0.138 \times 20 \times 300 \times 500^2$$

$$= 207 \text{ kNm}$$

$$\mu_{u \text{ max}} = 0.48 d = 0.48 \times 500 = 240 \text{ mm}$$

To find (μ_u)

$$0.36 F_{ck} b \mu_u + F_{sc} A_{sc} = 0.87 F_y A_{st}$$

$$= 2160 \mu_u + 119769.37 = 453706.26$$

$$= 2160 \mu_u = 453706.26 - 119769.37$$

$$= \mu_u = \frac{453706.26 - 119769.37}{2160}$$

$$2160$$

$$= 154.6 \text{ mm}$$

$\mu_u < \mu_{u \text{ max}}$ so the beam is under reinforced section.

$$M_{u2} = 0.36 f_{ck} b x_u (d - 0.42 x_u) + A_{sc} f_{sc} (d - d')$$

$$= 0.36 \times 20 \times 300 \times 154.6 (500 - 0.42 \times 154.6) +$$

$$339.29 \times 353 (500 - 40)$$

$$= 200 \text{ kNm}$$

Design of Shear

Shear force is present in beams where there is a change in bending moment along the span. It is equal to the rate of change of bending moment. So several experimental studies have been conducted to understand the various modes of failure, which occur due to possible combination of bending moment acting at a given section of shear &

These modes are as follows :-

- i) Diagonal tension failure
- ii) Flexural shear failure
- iii) Diagonal compression failure

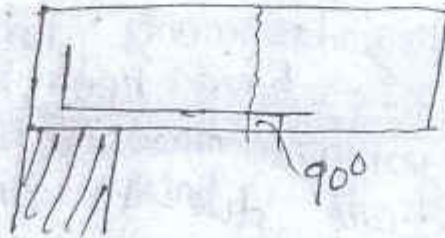
i) Diagonal tension failure :-

Diagonal tension failure which occurs under large shear force and less bending moment. Such cracks are normally at 45° with the horizontal.



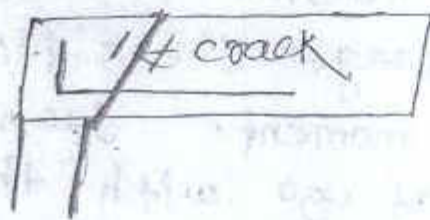
(ii) Flexural shear failure

Flexural shear failure which occurs under large bending moment & less shear force. Such cracks are normally at 90° with the horizontal.



(iii) Diagonal Compression failure

Diagonal compression failure which occurs under large shear force as shown in fig. normally it occurs in beams which are reinforced against heavy shear.



23 Jun 2021

Ultimate nominal stress (τ_v)

For a beam of uniform depth, the ultimate nominal shear stress τ_v is given by

$$\tau_v = \frac{V_u}{bd}$$

(page - 72)

where,

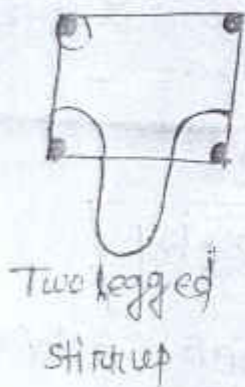
V_u = factored shear force due to load

Shear reinforcement in beam :-

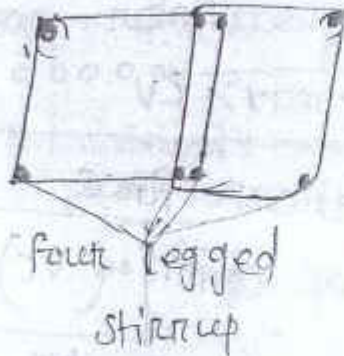
The shear reinforcement is made by any of the following forms.

- (i) vertical stirrup
- (ii) Inclined stirrup (not less than 45°)
- (iii) Bent up bars along with stirrup

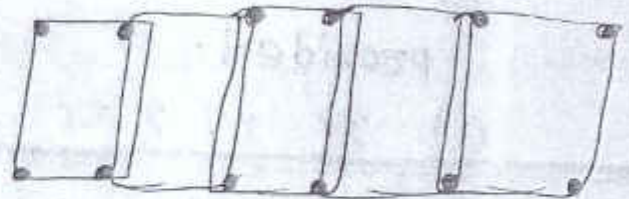
Type of stirrup :-



Two legged stirrup



four legged stirrup



six-legged stirrup

Bent up reinforcement to resist shear

Bent up bars along with stirrups must be used to resist shear. The shear resistance provided by bent up bars shouldn't be taken more than 50% of the total shear reinforcement required.

Design shear strength of conc. (τ_c)

(a) Without shear reinforcement. The design shear strength ' τ_c ' of conc. in beam without shear reinforcement.

(Code book - page no - 73 table no - 19)

b) With shear reinforcement

000
under no circumstances with shear reinforcement shall the nominal shear stress in beam exceeds $\tau_{c\max}$

(page - 73, table no - 20)

24 June 2021

NOTE :-

① If $\tau_v < \tau_c$, min^m shear reinforcement provided.

② If $\tau_v > \tau_c$, $\tau_{c\max} > \tau_v$

Let V_u = factored shear force

Shear resistance of conc. $(V_c) = \tau_c b d$

Net shear to be resisted by shear reinforcement = $V_{us} = V_u - V_c$

The strength of shear reinforcement V_{us} shall be calculated.

① For vertical stirrup

$$V_{us} = \frac{0.87 f_y A_s v d}{S_v}$$

② For inclined stirrup

$$V_{us} = \frac{0.87 f_y A_s v d (\sin \alpha + \cos \alpha)}{S_v}$$

(iii) For single bar or singly group of parallel bars, all bent up at the same cross section (c)

$$V_{us} = 0.87 f_y A_{sv} \sin \alpha$$

where, A_{sv} = total cross-sectional area of stirrup legs effective.

S_v = stirrup spacing along the length of the member.

α = Angle between inclined stirrup or bent up bar.

Min^m shear reinforcement

$$\frac{A_{sv}}{b s_v} = \frac{0.4}{0.87 f_y}$$

$$\Rightarrow S_v = \frac{A_{sv} 0.87 f_y}{0.4 b}$$

Max^m spacing of shear reinforcement

p shalln't be exceeded

① 300 mm

② 0.75d

0.8m

1Q A simply supported reinforced concrete beam is 250 mm wide & 500 mm effective depth & is reinforced with 5 bars of 18 mm as tensile steel. If the beam is subjected to factored shear of 62.5 kN at the support. Find the nominal shear stress at the supported & design shear reinforcement use M20 grade concrete & Fe 415 steel.

Solⁿ Given data :-

width of the beam = 250 mm

Effective depth = 500 mm

$$A_{st} = 5 \times \frac{\pi}{4} \times 18^2 = 1272.34 \text{ mm}^2$$

Factored shear $V_u = 62.5 \text{ kN}$

M20 grade $f_{ck} = 20 \text{ N/mm}^2$

Fe 415 $f_y = 415 \text{ N/mm}^2$

Step-1

$$\begin{aligned} \text{Nominal shear stress } (\tau_v) &= \frac{V_u}{bd} \\ &= \frac{62.5 \times 10^3}{250 \times 500} = 0.5 \text{ N/mm}^2 \end{aligned}$$

Step-2

$$\% \text{ of steel} = \frac{1272.34}{250 \times 500} \times 100 = 1\%$$

Step-III

For 1% steel, $\tau_c = 0.62 \text{ N/mm}^2$

$\tau_v < \tau_c$ so minimum shear reinforcement is provided.

Provide 6mm ϕ mild steel bars for stirrup of a legged stirrup.

$$\begin{aligned} S_v &= \frac{0.87 \times z_y A_{sv}}{\cancel{0.87} \times 0.4b} \\ &= \frac{0.87 \times 250 \times (2 \times \frac{\pi}{4} \times 6^2)}{0.4 \times 250} \\ &= 123.688 \text{ mm} \end{aligned}$$

S_v shall not be exceeded

① 300 mm

② $0.75d = 0.75 \times 500 = 375 \text{ mm}$

Provide two legged 6mm ϕ stirrup

(a) 123 mm c/c